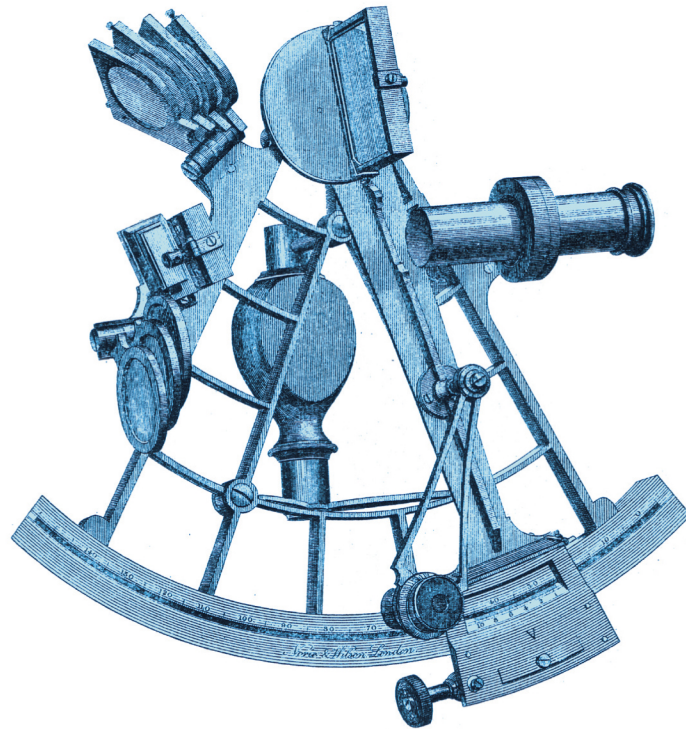


STARK TABLES

FOR
CLEARING THE LUNAR DISTANCE

AND

FINDING UNIVERSAL TIME BY SEXTANT OBSERVATION



INCLUDING
A CONVENIENT WAY TO SHARPEN
CELESTIAL NAVIGATION SKILLS WHILE ON LAND

BRUCE STARK

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Preface

These tables are the outcome of nearly two decades of experience with, and research into, the problem of getting Greenwich time from the moon. They reduce the calculation that clears a distance of refraction and parallax to a simple routine. The method fills a special niche. Unlike other easy-to-use procedures for clearing, it remains accurate when the distance is short. Short distances are the only ones the navigator of a quick-motined small boat can hope to measure with confidence.

Lunars were more important in navigation—and for a longer period—than is commonly recognized. It is true they became really practical only in 1767, the first year of the *Nautical Almanac*, and that by then John Harrison had already perfected his best timekeeper. But special “watches” such as Harrison’s were extremely difficult and expensive to build, and generations passed before they were standard equipment for ocean-going ships. On a long voyage a ship that did have a chronometer used it in conjunction with lunars.

Bowditch had more faith in lunars than in chronometers. Of longitude-by-chronometer he wrote:

This method is useful in a short run; but in a long voyage, implicit confidence cannot be place in an instrument of such a delicate construction, and liable to so many accidents.

And of longitude-by-lunar distance:

Other methods of finding the longitude at sea have been proposed, but among them all there is not one of such practical utility, as that by measuring the angular distance of the moon from the sun, or from certain fixed stars situated near the ecliptic, usually called a *lunar observation*, or, more frequently, “*a lunar*.”

(These quotes are from the 1851 edition of *The New American Practical Navigator*, page 225. Wording is different in the 1821 edition, page 148, but the message is the same.)

Although each 0.1 of error in the distance causes about twelve seconds of error in Greenwich time—3' of longitude—Bowditch had no trouble taking his ship from one place to another quickly and safely. He had a good idea what his maximum error in longitude could be at a given time, and allowed for it when shaping a course or making the land.

But by the middle of the nineteenth century chronometers were so reasonably priced that ships often carried three, and geography had improved to the point that almost any land raised served to check longitude. More and more steamships were being built—ships that couldn't be held up for weeks by a headwind or calm. Lunars were less and less needed. By the eighteen-nineties they were, as Captain Lecky put it in his *Wrinkles in Practical Navigation*, "... as dead as Julius Caesar."

Actually they weren't quite *that* dead. Joshua Slocum and a few others were still using them.

Now GPS is about to do for the rest of celestial navigation what chronometers and radio time signals did for the lunar. This might seem an awkward time for it, but if you enjoy using a sextant you will welcome the resurrection of the lunar distance. For one thing, lunars could help keep celestial navigation alive.

The present justification for celestial is that it provides a backup when electronics fail. The argument will have more force if lunars are part of the navigator's kit, since the electromagnetic shock wave from a nearby lightning strike can derange the timekeepers, even spring driven ones, in the same instant it takes out the electronics.

A more compelling point is this: Nothing else comes close to the lunar for developing skill with a sextant—and the observation is demanding enough to hold one's interest for a lifetime. On land a navigator who already knows his position can observe a distance on a moment's notice, day or night, without a horizon of any kind. When he compares his result with known GMT he will get the clean, reliable feedback he needs to continually improve his technique.

A third reason for resurrecting the lunar is to encourage more people to use sextants. At present it doesn't make sense to have a sextant unless you take it to sea. There's no other way to get enough satisfaction out of it to justify the price. Lunars will make land-based celestial navigation interesting enough to take up for its own sake, and amateur astronomers will find a sextant is worth owning.

The sextant doesn't belong exclusively to the sea. Explorers, geographers, and surveyors depended on sextants as they mapped the continental interiors. Not all these men are forgotten. Read a bit of history on the western two-thirds of the continent and you'll find references to Canada's intrepid David Thompson. And there are others. But of all the men who observed lunar distances on the river banks and in the mountain passes of the North American continent, the two best known—in the United States at least—are Lewis and Clark. The details of lunars are recorded in their journals.

Using the Tables

Three lunars are included as examples. One was measured from a planet, one from the sun, and one from a star. All were observed on land, but fake sea-horizon altitudes were used to clear the one on the opposite page. Height of eye is supposed to be eight feet.

Probably the quickest way to learn the method is to work the three examples for yourself. The blank forms bound into the book before the first table should be saved as patterns. Make photocopies as you need them. One form clears the distance, the other gets comparing distances (and GMT) when you have only the present-day *Nautical Almanac* to work with.

From the *Nautical Almanac*: Take the moon's H.P. for the hour you believe to be nearest the GMT of the observation. Put it in the box at the upper right corner of the form. If the distance was measured from Venus or Mars, check the bottom of page 259 in the *Almanac* to see if a value of "p." is given. If so, enter it above the moon's H.P. box. That's all you need from the *Almanac* for clearing.

To change sextant altitudes to apparent altitudes of the centers: If you have sextant altitudes for the moment of the distance, put them in the spaces on the top row. Circle the figure that best represents the body and limb you brought to the horizon.

There is no place on the form to adjust sextant altitudes for index and instrument error, since these are usually small, and altitudes not critical. But if combined index and instrument error amounts to 1' or more it might be worthwhile correcting for them before putting the altitudes on the form.

Next, enter Table 1. Find your height-of-eye at the top and go down the column to the row of best fit. Take out an adjustment, together with + or - sign, for each of the altitudes. Apply these and you have **Sa** and **Ma**. Unorthodox symbols are used because, in present-day navigation, "H_a" refers to the sun's or moon's limb. These are apparent altitudes of the centers.

To change calculated altitudes: Since these are true altitudes you have to put parallax and refraction *into* them to get **Ma** and **Sa**. The W.W. (Wrong Way) tables give these adjustments, together with + or - signs for applying them. You will find examples on page 9, facing the W.W. Ref. Table.



Put the resulting **Sa** and **Ma** directly on the form, leaving the first two lines blank, as will be shown in the next example.

Refraction, parallax, and "Q": On the form, follow the arrow to the right of **Ma** and enter Table 2. In Table 2 the headings of both columns and rows are at 2' intervals. That's close enough for **Ma**. Use the *nearest* value. But if there isn't an exact match for H.P. use the column headed by the next *lesser* value. Then copy increments from the table in the margin onto the next line of the form.

Move on to Table 3 and take out r&p and Q for the other body's altitude. The hundredths of a minute of arc in refraction and parallax are there so when parts are added there will be no rounding error in the tenths. The figure to the right of the comma in the Q function has a similar purpose. Don't interpolate between values. All the way through this system values are tabulated to the precision needed. Interpolation would be a waste of time. The only exception is that part of the "K" table above 104°, and it is seldom used.

Add the three lines. Q will be needed on the fourth line from the bottom. It's a negative logarithm of the ratio of cosines of true and apparent altitudes, if you are curious. But the method is designed for navigators who know nothing about trigonometry or logarithms. Those who happen to know about such

h. eye 8 ft.

| | | | |
|---|----------|---|----------|
|  | 27° 52.5 |  | 23° 38.0 |
| Table 1 | - 2.7 | Table 1 | + 12.5 |
| ♀ Sa | 27° 49.8 | Ma | 23° 50.5 |
| (subtract lesser) | 23° 50.5 | or | |
| Ma~Sa | 3° 59.3 | | |
| | - 51.0 | + | (round) |
| H~H | 3° 8.3 | | |

from Almanac, the moon's H.P. = $\frac{0.1}{56.2}$

| | | |
|---------|-------|-------|
| Table 2 | 48.14 | 261.5 |
| | 1.10 | 6.3 |
| Table 3 | 1.73 | 0.6 |
| | 50.97 | 268.4 |
| | | Q |

| | | |
|-----------------------|---------|--------------|
| | off + | on - |
| Index error | . | .2 |
| Instrument | . | . |
| Moon's Limb Near? | . | 15.4 or Far? |
| Ds (Sextant Distance) | 4° 19.1 | 15.6 |
| | | -15.6 |
| Da | 4° 3.5 | |
| Ma~Sa | 3° 59.3 | |
| Da - (Ma~Sa) | 0° 4.2 | |
| Da + (Ma~Sa) | 8° 2.8 | |

| | | |
|--------------------|-------|-------|
| Table 4 | 15.42 | } add |
| SUN ? 5 | . | |
| LOW sun or moon? 6 | -. | |
| (round) | . | |

| | | | | | |
|-----|---------|------|-----------------|----------------|-------------------|
| H-H | 3° 8.3 | K | 3.12 | 502 | } add |
| | | | .02 | 400 | |
| D | 3° 13.6 | ⊗ | 3.10 | 102 | (subtract lesser) |
| | | | 8.73 | 590 | } add |
| | | half | 4.36 | 795.0 | |
| | | Q | | 268.4 | |
| | | | 4.37 | 063 | (round) |
| | | or | 3.12 | 502 | |
| | | | 1.24 | 561 | |

date: Nov 8 '96 GMT
 Previous Hour: 14

♀

G.H.A. 66° 6.5
 G.H.A. 64° 3.0
 difference 2° 3.5

STAR: S.H.A. ° .
 G.H.A. Aries ° . } add
 ° .
-3 6 0 ?

Dec. (N. or S?) 5° 15.7 -----> log Dec. -----> .00 183
 Dec. (N. or S?) 3° 14.3 -----> log Dec. -----> . 069

difference 2° 1.4 K 3.50 622 <-> 3.49 384
 D 3 13.6 3.49 384 or .29 489 (subtract lesser)
 D#1 2° 52.9 0.01 238 3.19 895
20.7

date: _____ GMT
 Following Hour: _____

G.H.A. 81° 6.2
 G.H.A. 78° 34.8
 difference 2° 31.4

STAR: S.H.A. ° .
 G.H.A. Aries ° . } add
 ° .
-3 6 0 ?

Dec. (N. or S?) 5° 25.3 -----> log Dec. -----> . 195
 Dec. (N. or S?) 3° 15.4 -----> log Dec. -----> . 070

difference 2° 9.9 K 3.44 744 <-> 3.31 708 (subtract lesser)
 D#2 3° 19.2 3.31 708 or .24 072
2 52.9
26.3

Table

D ~ D#1 20.7 7 1.06 42
 D#2 ~ D#1 26.3 7 -0.96 03

8 0.1 039 47 min. 14 sec.
 True: 47 01
 error = 13

0.96 03
2.44 24
3.40 27
 0.1 Gap in contact

Since they are about the same altitude, the moon and other body are affected equally by refraction. But the star or planet has little or no parallax, while the moon has a lot. She appears lower in the sky than she would otherwise. To get an idea where the *Almanac* puts the moon in relation to the star or planet, use her own diameter as a gauge. If the altitude is around 5° imagine her two diameters higher; if around 30° , one and a half diameters; around 60° , one diameter; 75° , a half.

If someone publishes an almanac, or list, of comparing distances we can look at the list to see what bodies are suitable from the *Almanac's* point of view. But whether or not an extremely short distance is also worth taking from *our* point of view will still have to be judged by eye, as that will depend on where—on the surface of the globe—we happen to be.

Another problem with short distances has to do with interpolating for GMT. In the first example—the Venus observation—the $3^\circ 13.6'$ distance got a GMT of 14:47:14. But that was based on the supposition the distance was changing at the same rate all through the hour, from 14:00 to 15:00. It wasn't. Venus was about 30° out of line with the moon's orbital motion, and alignment was changing during the hour. When a distance is that short the moon's half degree of progress along her orbit makes a difference. The amount the star or planet is out of line increases or decreases, and change in distance slows down or speeds up accordingly.

If, in the Venus example, this "second difference" in rate of change is allowed for, GMT is found to be 14:47:25. But to allow for it I had, among other things, to calculate the distance for 13:00. In my opinion second differences are not worth bothering with—not so long as we must calculate our own comparing distances, at least. The effect is greatest at the half hour, so you can limit the problem by taking your observation near the beginning or end of the hour.

Second differences were *nine times* as much of a nuisance in Bowditch's day. The maximum error they can cause is proportional to the square of the interval between comparing distances, and the interval in the *Almanac* was three hours. Consequently, distances less than 20° were seldom listed. It didn't matter then that the popular methods of clearing fell apart below 20° . When Bowditch spoke of short distances he was probably thinking of those under 50° .

Degree of fussiness: This is the measure of one's willingness to agonize over details for the sake of a little more accuracy—details such as second differences, the effect of refraction on the shape of the sun's or moon's disk (table 6), the effects of temperature and pressure on refraction, and the effects of the oblate shape of the earth on parallax and vertical plane.

No doubt there were people who took all these things into account. Certainly it would have made sense for those surveyors who provided themselves with tripods to mount their sextants or circles on. But the evidence I've come across so far suggests these details were almost universally ignored. In Bowditch's opinion it was best to skip all such embellishments and use the time saved to take observations more often.

I put table 6 in because the correction is easy to use and not apt to cause a blunder. But if the other refinements are dealt with it will be in a pamphlet, to keep them separate from these tables.

Sample Workform for Clearing the Lunar Distance

Aldeb.

| | |
|--------------------|---------------------------|
| | |
| Table 1 | Table 1 |
| Sa <u>31° 19.4</u> | Ma <u>57° 39.4</u> -----> |
| (subtract lesser) | or <u>31° 19.4</u> |
| Ma~Sa | <u>26° 20.0</u> |
| - | + 30.2 (round) |
| H~H | <u>26° 50.2</u> |

from Almanac, the moon's H.P. = 54.6

| | |
|---------|-------------------------------|
| Table 2 | { <u>27.74</u> <u>546.5</u> |
| | .86 17.4 |
| Table 3 | { <u>1.58</u> <u>0.0</u> |
| | ← <u>30.18</u> <u>563.9</u> |

| | | | |
|-------------------|-------|------|---------|
| | off + | | on - |
| Index error | . | . | .2 |
| Instrument | . | . | . |
| Moon's Limb Near? | . | 15.1 | or Far? |

Ds (Sextant Distance) → 40° 37.6 | 15.3

-15.3 ←

Da 40° 22.3

Ma~Sa 26° 20.0

Da - (Ma~Sa) 14° 2.3 -----> K 1.82 | 585 } add

Da + (Ma~Sa) 66° 42.3 -----> K 0.51 | 961 } add

2.34 | 546

half ↓ 1.17 | 273.0 } add

Q 563.9

H~H 26° 50.2 K 1.26 | 880 } (round)

or 1.17 | 837 } (subtract lesser)

D 40° 34.0 0.09 | 043 } 0.92 | 020

Example of Adjusting Altitudes to an Intermediate Time

| | |
|------|-------------|
| Date | May 7, 2000 |
|------|-------------|

| | |
|------|-----|
| Body | Sun |
|------|-----|

Elapsed Time between 1st Altitude and Time of Lunar Distance Observation

| | | | | |
|----------------------------------|-------------|---------|---|--------|
| Time of 1 st Altitude | 23h 03m 49s | | | |
| Time of Lunar Distance Obs. | 23h 08m 43s | | | |
| Difference | 00h 04m 54s | Table 8 | 1 | 1.0894 |

Elapsed time Between 1st Altitude and Last Altitude

| | | | | |
|----------------------------------|-------------|---------|---|--------|
| Time of 1 st Altitude | 23h 03m 49s | | | |
| Time of Last Altitude. | 23h 12m 30s | | | |
| Difference | 00h 08m 41s | Table 8 | 2 | 0.8395 |

| | | |
|-------------------|---|--------|
| Subtract 2 from 1 | 3 | 0.2499 |
|-------------------|---|--------|

Change in Altitude Between 1st and Last Observation

| | | | | |
|-----------------------------------|-----------|---------|---|--------|
| 1 st Observed Altitude | 42° 36.3' | | | |
| Last Observed Altitude. | 41° 16.0' | | | |
| Difference | 01° 20.3' | Table 7 | 4 | 0.4755 |

| | | |
|--------------|---|--------|
| Add 3 and 4, | 5 | 0.7254 |
|--------------|---|--------|

| | |
|---|-----------|
| Enter argument 5 into Table 7 , extract value, then add or subtract to 1 st observed altitude | 00° 45.2' |
|---|-----------|

| | |
|---|------------|
| 1 st Observed Altitude | 42° 36.3' |
| Increment to be Added to or Subtracted from, 1 st Altitude Observation | -00° 45.2' |
| Observed Altitude adjusted to common time | 41° 51.1' |

Courtesy of Robert Eno, Iqaluit, NT

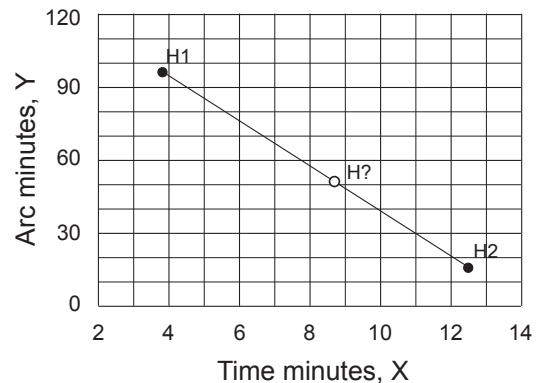
A sun-moon lunar distance was measured at 23h 08m 43s. The sun altitude was measured first at 23h 03m 49s, which gave H1 = 42° 36.3' (plotted as 41° 96.3'), and then measured again at 23h 12m 30s, which gave H2 = 41° 16.0'.

Use the work form to find the precise value of the sun altitude (H?) at 23h 08m 43s, the time of the lunar.

In the plot:

Sight Time = 23 hr + X time min

Sextant Altitude = 41° + Y arc min



W.W.P. Moon

W.W.P. Moon

To get 'Ma' from a CALCULATED altitude of the moon, apply this, then W.W.Ref. (Skip Table 1)

| From N. Almanac H.P. | 67° | | | 68° | | | 69° | | | 70° | | | 71° | | | 72° | | | 73° | | | 74° | | |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | 0' | 20' | 40' | 0' | 20' | 40' | 0' | 20' | 40' | 0' | 20' | 40' | 0' | 20' | 40' | 0' | 20' | 40' | 0' | 20' | 40' | 0' | 20' | 40' |
| 54.0 | -21.4 | -21.1 | -20.8 | -20.5 | -20.2 | -19.9 | -19.6 | -19.3 | -19.0 | -18.7 | -18.4 | -18.1 | -17.8 | -17.5 | -17.2 | -16.9 | -16.6 | -16.3 | -16.0 | -15.7 | -15.4 | -15.1 | -14.8 | -14.5 |
| .2 | -21.5 | -21.2 | -20.9 | -20.6 | -20.3 | -20.0 | -19.7 | -19.4 | -19.1 | -18.8 | -18.5 | -18.2 | -17.9 | -17.6 | -17.3 | -17.0 | -16.7 | -16.4 | -16.1 | -15.8 | -15.5 | -15.2 | -14.9 | -14.6 |
| .4 | -21.6 | -21.3 | -21.0 | -20.7 | -20.4 | -20.1 | -19.8 | -19.5 | -19.2 | -18.9 | -18.6 | -18.3 | -18.0 | -17.7 | -17.4 | -17.1 | -16.8 | -16.5 | -16.2 | -15.9 | -15.6 | -15.3 | -15.0 | -14.7 |
| .6 | -21.6 | -21.3 | -21.1 | -20.8 | -20.5 | -20.2 | -19.9 | -19.6 | -19.3 | -19.0 | -18.7 | -18.4 | -18.1 | -17.8 | -17.5 | -17.2 | -16.9 | -16.6 | -16.3 | -16.0 | -15.7 | -15.4 | -15.0 | -14.7 |
| .8 | -21.7 | -21.4 | -21.1 | -20.8 | -20.5 | -20.2 | -19.9 | -19.7 | -19.4 | -19.1 | -18.8 | -18.5 | -18.2 | -17.9 | -17.6 | -17.3 | -17.0 | -16.6 | -16.3 | -16.0 | -15.7 | -15.4 | -14.8 | -14.7 |
| 55.0 | -21.8 | -21.5 | -21.2 | -20.9 | -20.6 | -20.3 | -20.0 | -19.7 | -19.4 | -19.1 | -18.8 | -18.5 | -18.2 | -17.9 | -17.6 | -17.3 | -17.0 | -16.6 | -16.3 | -16.0 | -15.7 | -15.4 | -14.8 | -14.8 |
| .2 | -21.9 | -21.6 | -21.3 | -21.0 | -20.7 | -20.4 | -20.1 | -19.8 | -19.5 | -19.2 | -18.9 | -18.6 | -18.2 | -17.9 | -17.6 | -17.3 | -17.0 | -16.7 | -16.4 | -16.1 | -15.8 | -15.4 | -15.1 | -14.8 |
| .4 | -22.0 | -21.7 | -21.4 | -21.1 | -20.8 | -20.5 | -20.2 | -19.9 | -19.6 | -19.2 | -18.9 | -18.6 | -18.3 | -18.0 | -17.7 | -17.4 | -17.1 | -16.8 | -16.4 | -16.1 | -15.8 | -15.5 | -15.2 | -14.9 |
| .6 | -22.0 | -21.7 | -21.4 | -21.1 | -20.8 | -20.5 | -20.2 | -19.9 | -19.6 | -19.3 | -19.0 | -18.7 | -18.4 | -18.1 | -17.8 | -17.4 | -17.1 | -16.8 | -16.5 | -16.2 | -15.9 | -15.6 | -15.2 | -14.9 |
| .8 | -22.1 | -21.8 | -21.5 | -21.2 | -20.9 | -20.6 | -20.3 | -20.0 | -19.7 | -19.4 | -19.1 | -18.8 | -18.4 | -18.1 | -17.8 | -17.5 | -17.2 | -16.9 | -16.6 | -16.3 | -16.0 | -15.7 | -15.3 | -15.0 |
| 56.0 | -22.2 | -21.9 | -21.6 | -21.3 | -21.0 | -20.7 | -20.4 | -20.1 | -19.8 | -19.4 | -19.1 | -18.8 | -18.5 | -18.2 | -17.9 | -17.6 | -17.3 | -17.0 | -16.6 | -16.3 | -16.0 | -15.7 | -15.4 | -15.0 |
| .2 | -22.3 | -22.0 | -21.7 | -21.4 | -21.1 | -20.8 | -20.4 | -20.1 | -19.8 | -19.5 | -19.2 | -18.9 | -18.6 | -18.3 | -18.0 | -17.6 | -17.3 | -17.0 | -16.7 | -16.4 | -16.1 | -15.7 | -15.4 | -15.1 |
| .4 | -22.4 | -22.1 | -21.8 | -21.4 | -21.1 | -20.8 | -20.5 | -20.2 | -19.9 | -19.6 | -19.3 | -19.0 | -18.6 | -18.3 | -18.0 | -17.7 | -17.4 | -17.1 | -16.7 | -16.4 | -16.1 | -15.8 | -15.5 | -15.1 |
| .6 | -22.4 | -22.1 | -21.8 | -21.5 | -21.2 | -20.9 | -20.6 | -20.3 | -20.0 | -19.7 | -19.3 | -19.0 | -18.7 | -18.4 | -18.1 | -17.8 | -17.4 | -17.1 | -16.8 | -16.5 | -16.2 | -15.8 | -15.5 | -15.2 |
| .8 | -22.5 | -22.2 | -21.9 | -21.6 | -21.3 | -21.0 | -20.7 | -20.4 | -20.0 | -19.7 | -19.4 | -19.1 | -18.8 | -18.5 | -18.1 | -17.8 | -17.5 | -17.2 | -16.9 | -16.6 | -16.2 | -15.9 | -15.6 | -15.3 |
| 57.0 | -22.6 | -22.3 | -22.0 | -21.7 | -21.4 | -21.1 | -20.7 | -20.4 | -20.1 | -19.8 | -19.5 | -19.2 | -18.8 | -18.5 | -18.2 | -17.9 | -17.6 | -17.3 | -17.0 | -16.6 | -16.3 | -16.0 | -15.6 | -15.3 |
| .2 | -22.7 | -22.4 | -22.1 | -21.8 | -21.4 | -21.1 | -20.8 | -20.5 | -20.2 | -19.9 | -19.6 | -19.2 | -18.9 | -18.6 | -18.3 | -18.0 | -17.6 | -17.3 | -17.0 | -16.7 | -16.3 | -16.0 | -15.6 | -15.3 |
| .4 | -22.8 | -22.5 | -22.1 | -21.8 | -21.5 | -21.2 | -20.9 | -20.6 | -20.3 | -19.9 | -19.6 | -19.3 | -19.0 | -18.7 | -18.3 | -18.0 | -17.7 | -17.4 | -17.0 | -16.7 | -16.3 | -16.0 | -15.7 | -15.4 |
| .6 | -22.9 | -22.5 | -22.2 | -21.9 | -21.6 | -21.3 | -21.0 | -20.6 | -20.3 | -20.0 | -19.7 | -19.4 | -19.0 | -18.7 | -18.4 | -18.1 | -17.8 | -17.4 | -17.1 | -16.8 | -16.5 | -16.1 | -15.8 | -15.5 |
| .8 | -22.9 | -22.6 | -22.3 | -22.0 | -21.7 | -21.4 | -21.1 | -20.8 | -20.5 | -20.1 | -19.8 | -19.4 | -19.1 | -18.8 | -18.5 | -18.1 | -17.8 | -17.5 | -17.2 | -16.9 | -16.5 | -16.2 | -15.9 | -15.6 |
| 58.0 | -23.0 | -22.7 | -22.4 | -22.1 | -21.8 | -21.4 | -21.1 | -20.8 | -20.5 | -20.2 | -19.8 | -19.5 | -19.2 | -18.9 | -18.5 | -18.2 | -17.9 | -17.6 | -17.3 | -17.0 | -16.6 | -16.3 | -16.0 | -15.6 |
| .2 | -23.1 | -22.8 | -22.5 | -22.2 | -21.9 | -21.5 | -21.2 | -20.9 | -20.5 | -20.2 | -19.9 | -19.6 | -19.3 | -19.0 | -18.6 | -18.3 | -18.0 | -17.6 | -17.3 | -17.0 | -16.6 | -16.3 | -16.0 | -15.6 |
| .4 | -23.2 | -22.9 | -22.5 | -22.2 | -21.9 | -21.6 | -21.3 | -21.0 | -20.6 | -20.3 | -20.0 | -19.6 | -19.3 | -19.0 | -18.7 | -18.3 | -18.0 | -17.7 | -17.4 | -17.0 | -16.7 | -16.4 | -16.0 | -15.7 |
| .6 | -23.3 | -22.9 | -22.6 | -22.3 | -22.0 | -21.7 | -21.3 | -21.0 | -20.7 | -20.4 | -20.0 | -19.7 | -19.4 | -19.1 | -18.7 | -18.4 | -18.1 | -17.7 | -17.4 | -17.0 | -16.7 | -16.4 | -16.1 | -15.8 |
| .8 | -23.3 | -23.0 | -22.7 | -22.4 | -22.1 | -21.7 | -21.4 | -21.1 | -20.8 | -20.4 | -20.1 | -19.8 | -19.5 | -19.1 | -18.8 | -18.5 | -18.1 | -17.8 | -17.5 | -17.2 | -16.9 | -16.5 | -16.2 | -15.8 |
| 59.0 | -23.4 | -23.1 | -22.8 | -22.5 | -22.1 | -21.8 | -21.5 | -21.2 | -20.8 | -20.5 | -20.2 | -19.8 | -19.5 | -19.2 | -18.9 | -18.5 | -18.2 | -17.9 | -17.5 | -17.2 | -16.9 | -16.5 | -16.2 | -15.9 |
| .2 | -23.5 | -23.2 | -22.9 | -22.5 | -22.2 | -21.9 | -21.6 | -21.2 | -20.9 | -20.6 | -20.2 | -19.9 | -19.6 | -19.3 | -18.9 | -18.6 | -18.3 | -17.9 | -17.6 | -17.3 | -17.0 | -16.6 | -16.3 | -15.9 |
| .4 | -23.6 | -23.3 | -22.9 | -22.6 | -22.3 | -22.0 | -21.6 | -21.3 | -21.0 | -20.6 | -20.3 | -20.0 | -19.7 | -19.3 | -19.0 | -18.7 | -18.3 | -18.0 | -17.7 | -17.3 | -17.0 | -16.6 | -16.3 | -16.0 |
| .6 | -23.7 | -23.3 | -23.0 | -22.7 | -22.4 | -22.0 | -21.7 | -21.4 | -21.0 | -20.7 | -20.4 | -20.1 | -19.7 | -19.4 | -19.1 | -18.7 | -18.4 | -18.1 | -17.7 | -17.4 | -17.0 | -16.7 | -16.4 | -16.0 |
| .8 | -23.7 | -23.4 | -23.1 | -22.8 | -22.4 | -22.1 | -21.8 | -21.4 | -21.1 | -20.8 | -20.5 | -20.1 | -19.8 | -19.5 | -19.1 | -18.8 | -18.4 | -18.1 | -17.8 | -17.4 | -17.1 | -16.8 | -16.4 | -16.1 |
| 60.0 | -23.8 | -23.5 | -23.2 | -22.8 | -22.5 | -22.2 | -21.9 | -21.5 | -21.2 | -20.9 | -20.5 | -20.2 | -19.9 | -19.5 | -19.2 | -18.8 | -18.5 | -18.2 | -17.8 | -17.5 | -17.2 | -16.8 | -16.5 | -16.1 |
| .2 | -23.9 | -23.6 | -23.2 | -22.9 | -22.6 | -22.3 | -22.0 | -21.6 | -21.3 | -20.9 | -20.6 | -20.3 | -19.9 | -19.6 | -19.3 | -18.9 | -18.6 | -18.2 | -17.9 | -17.6 | -17.2 | -16.9 | -16.5 | -16.2 |
| .4 | -24.0 | -23.7 | -23.3 | -23.0 | -22.7 | -22.3 | -22.0 | -21.7 | -21.3 | -21.0 | -20.7 | -20.3 | -20.0 | -19.7 | -19.3 | -19.0 | -18.6 | -18.3 | -18.0 | -17.6 | -17.3 | -16.9 | -16.6 | -16.2 |
| .6 | -24.1 | -23.7 | -23.4 | -23.1 | -22.7 | -22.4 | -22.1 | -21.7 | -21.4 | -21.1 | -20.7 | -20.4 | -20.1 | -19.7 | -19.4 | -19.0 | -18.7 | -18.4 | -18.0 | -17.7 | -17.3 | -17.0 | -16.6 | -16.3 |
| .8 | -24.1 | -23.8 | -23.5 | -23.1 | -22.8 | -22.5 | -22.1 | -21.8 | -21.5 | -21.1 | -20.8 | -20.5 | -20.1 | -19.8 | -19.4 | -19.1 | -18.8 | -18.4 | -18.1 | -17.7 | -17.4 | -17.0 | -16.7 | -16.4 |
| 61.0 | -24.2 | -23.9 | -23.6 | -23.2 | -22.9 | -22.6 | -22.2 | -21.9 | -21.5 | -21.2 | -20.9 | -20.5 | -20.2 | -19.9 | -19.5 | -19.2 | -18.8 | -18.5 | -18.1 | -17.8 | -17.4 | -17.1 | -16.8 | -16.4 |
| .2 | -24.3 | -24.0 | -23.6 | -23.3 | -23.0 | -22.6 | -22.3 | -22.0 | -21.6 | -21.3 | -20.9 | -20.6 | -20.3 | -19.9 | -19.6 | -19.2 | -18.9 | -18.5 | -18.2 | -17.9 | -17.5 | -17.2 | -16.8 | -16.5 |
| .4 | -24.4 | -24.1 | -23.7 | -23.4 | -23.1 | -22.7 | -22.4 | -22.0 | -21.7 | -21.4 | -21.0 | -20.7 | -20.3 | -20.0 | -19.6 | -19.3 | -19.0 | -18.6 | -18.3 | -17.9 | -17.6 | -17.2 | -16.9 | -16.5 |

W.W.P. Moon

To get "Ma" from a CALCULATED altitude of the moon, apply this, then W.W.Ref. (Skip Table 1)

| From N. Almanac H.P. | Calculated Altitude of Moon | | | | | | | | | | | | | | | | | | | | |
|----------------------------|-----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| | 83° | | 84° | | 85° | | 86° | | 87° | | 88° | | 89° | | | | | | | | |
| | 0' | 20' | 0' | 20' | 0' | 20' | 0' | 20' | 0' | 20' | 0' | 20' | 0' | 20' | | | | | | | |
| 54.0 | -6.7 | -6.4 | -5.7 | -5.4 | -5.1 | -4.8 | -4.5 | -4.1 | -3.8 | -3.5 | -3.2 | -2.9 | -2.6 | -2.2 | -1.9 | -1.6 | -1.3 | -1.0 | -0.6 | -0.3 | |
| 55.0 | -6.8 | -6.5 | -5.8 | -5.5 | -5.2 | -4.9 | -4.5 | -4.2 | -3.9 | -3.6 | -3.2 | -2.9 | -2.6 | -2.3 | -1.9 | -1.6 | -1.3 | -1.0 | -0.7 | -0.3 | |
| 56.0 | -6.9 | -6.6 | -5.9 | -5.6 | -5.3 | -5.0 | -4.6 | -4.3 | -4.0 | -3.6 | -3.3 | -3.0 | -2.6 | -2.3 | -2.0 | -1.7 | -1.3 | -1.0 | -0.7 | -0.3 | |
| 57.0 | -7.1 | -6.7 | -6.1 | -5.7 | -5.4 | -5.0 | -4.7 | -4.4 | -4.0 | -3.7 | -3.4 | -3.0 | -2.7 | -2.4 | -2.0 | -1.7 | -1.3 | -1.0 | -0.7 | -0.3 | |
| 58.0 | -7.2 | -6.8 | -6.2 | -5.8 | -5.5 | -5.1 | -4.8 | -4.5 | -4.1 | -3.8 | -3.4 | -3.1 | -2.7 | -2.4 | -2.1 | -1.7 | -1.4 | -1.0 | -0.7 | -0.3 | |
| 59.0 | -7.3 | -7.0 | -6.6 | -6.3 | -5.9 | -5.6 | -5.2 | -4.9 | -4.5 | -4.2 | -3.8 | -3.5 | -3.1 | -2.8 | -2.4 | -2.1 | -1.7 | -1.4 | -1.0 | -0.7 | -0.3 |
| 60.0 | -7.4 | -7.1 | -6.7 | -6.4 | -6.0 | -5.7 | -5.3 | -5.0 | -4.6 | -4.3 | -3.9 | -3.5 | -3.2 | -2.8 | -2.5 | -2.1 | -1.8 | -1.4 | -1.1 | -0.7 | -0.4 |
| 61.0 | -7.6 | -7.2 | -6.8 | -6.5 | -6.1 | -5.8 | -5.4 | -5.1 | -4.7 | -4.3 | -4.0 | -3.6 | -3.2 | -2.9 | -2.5 | -2.2 | -1.8 | -1.4 | -1.1 | -0.7 | -0.4 |

W.W.P. Venus or Mars

Don't bother with this unless you have reason to want an unusually precise calculated apparent altitude.

If Venus or Mars has parallax (p) of 0.1 or more any time during the year the Nautical Almanac gives it at the bottom of Page 259.

To get "Sa" from a CALCULATED Altitude of Venus or Mars apply this and W.W.Ref. (Skip Table 1)

| P | Calculated Altitude of Venus or Mars | | | | | | | | | | | | | | | | | | |
|-----|--------------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|-----|-----|
| | 5° | 10° | 15° | 20° | 25° | 30° | 35° | 40° | 45° | 50° | 55° | 60° | 65° | 70° | 75° | 80° | 85° | | |
| 0.1 | -0.1 | -0.1 | -0.1 | -0.1 | -0.1 | -0.1 | -0.1 | -0.1 | -0.1 | -0.1 | -0.1 | -0.1 | -0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| 0.2 | -0.2 | -0.2 | -0.2 | -0.2 | -0.2 | -0.2 | -0.2 | -0.2 | -0.1 | -0.1 | -0.1 | -0.1 | -0.1 | -0.1 | -0.1 | -0.1 | 0.0 | 0.0 | 0.0 |
| 0.3 | -0.3 | -0.3 | -0.3 | -0.3 | -0.3 | -0.2 | -0.2 | -0.2 | -0.2 | -0.2 | -0.2 | -0.2 | -0.1 | -0.1 | -0.1 | -0.1 | -0.1 | 0.0 | 0.0 |
| 0.4 | -0.4 | -0.4 | -0.4 | -0.4 | -0.4 | -0.3 | -0.3 | -0.3 | -0.3 | -0.3 | -0.3 | -0.2 | -0.2 | -0.2 | -0.1 | -0.1 | -0.1 | 0.0 | 0.0 |
| 0.5 | -0.5 | -0.5 | -0.5 | -0.5 | -0.5 | -0.4 | -0.4 | -0.4 | -0.4 | -0.4 | -0.3 | -0.3 | -0.2 | -0.2 | -0.2 | -0.1 | -0.1 | 0.0 | 0.0 |

Changing calculated altitudes to Ma and Sa, the apparent altitudes of the centers

Moon

$$\begin{array}{r} \text{Calculated Altitude: } 30^\circ 23.8 \\ \text{W.W.P. Moon Table: } \underline{-49.7} \\ \text{(H.P.=57.2)} \quad \swarrow \\ \quad \quad \quad \underline{29 \ 34.1} \\ \text{W.W. Ref. Table: } \underline{\quad + 1.7} \\ \quad \quad \quad \text{Ma} = 29^\circ 35.8 \end{array}$$

$$\begin{array}{r} \text{Sun, Star, or Planet} \\ \text{Calculated Altitude: } 45^\circ 31.2 \\ \text{W.W. Ref. Table: } \underline{\quad + 0.9} \\ \quad \quad \quad \text{Sa} = 45^\circ 32.1 \end{array}$$

The W.W.P. Moon table has rows for H.P. as close as needed. When H.P. falls between row headings you can use *either* row. If H.P. had been 57.1 in the example you could have taken either -49.5 or -49.7 as the adjustment.

For altitudes above 9° 51' W.W. Ref. is a critical table. This means that when an altitude falls between two values in the table you should use the adjustment shown for the space between them. But when it fits one of the values in the table *exactly*, use the adjustment given for the space above. This is the same rule you use with critical tables in the front of the *Nautical Almanac*.

Add to Calculated altitude (Hc) to get Ma or Sa. For the moon, first reduce Hc with W.W.P Moon before using it to enter this table.

| | | | | | | | | | | | | | |
|----|--------|-------|--------|------|----|---------|------|----|---------|----|---------|----|---------|
| Hc | 4° 0' | +11.3 | 6° 30' | +7.8 | Hc | 9° 51' | +5.3 | Hc | 13° 50' | Hc | 22° 16' | Hc | 48° 41' |
| | 4° 5' | +11.2 | 6° 35' | +7.7 | | 10° 3' | | | 14° 14' | | 23° 12' | | 52° 13' |
| | 4° 10' | +11.0 | 6° 40' | +7.6 | | 10° 15' | +5.2 | | 14° 36' | | 24° 10' | | 56° 5' |
| | 4° 15' | +10.9 | 6° 45' | +7.5 | | 10° 27' | +5.1 | | 15° 0' | | 25° 12' | | 60° 21' |
| | 4° 20' | +10.7 | 6° 50' | +7.4 | | 10° 41' | +5.0 | | 15° 27' | | 26° 18' | | 65° 2' |
| | 4° 25' | +10.6 | 6° 55' | +7.4 | | 10° 55' | +4.9 | | 15° 55' | | 27° 34' | | 70° 6' |
| | 4° 30' | +10.4 | 7° 0' | +7.3 | | 11° 9' | +4.8 | | 16° 23' | | 28° 54' | | 75° 30' |
| | 4° 35' | +10.3 | 7° 5' | +7.2 | | 11° 25' | +4.7 | | 16° 53' | | 30° 22' | | 81° 12' |
| | 4° 40' | +10.1 | 7° 10' | +7.1 | | 11° 39' | +4.6 | | 17° 25' | | 31° 58' | | 87° 0' |
| | 4° 45' | +10.0 | 7° 15' | +7.1 | | 11° 58' | +4.5 | | 17° 59' | | 33° 43' | | 90° |
| | 4° 50' | +9.9 | 7° 20' | +7.0 | | 12° 14' | +4.4 | | 18° 35' | | 35° 37' | | |
| | 4° 55' | +9.7 | 7° 25' | +6.9 | | 12° 32' | +4.3 | | 19° 15' | | 37° 43' | | |
| | 5° 0' | +9.6 | 7° 30' | +6.9 | | 12° 50' | +4.2 | | 19° 55' | | 40° 3' | | |
| | 5° 5' | +9.5 | 7° 35' | +6.8 | | 13° 10' | +4.1 | | 20° 39' | | 42° 39' | | |
| | 5° 10' | +9.4 | 7° 40' | +6.7 | | 13° 30' | +4.0 | | 21° 26' | | 45° 31' | | |
| | 5° 15' | +9.2 | 7° 45' | +6.7 | | 13° 50' | +3.9 | | 22° 16' | | 48° 41' | | |
| | 5° 20' | +9.1 | 7° 50' | +6.6 | | | | | | | | | |
| | 5° 25' | +9.0 | 7° 55' | +6.5 | | | | | | | | | |
| | 5° 30' | +8.9 | 8° 0' | +6.5 | | | | | | | | | |
| | 5° 35' | +8.8 | 8° 10' | +6.4 | | | | | | | | | |
| | 5° 40' | +8.7 | 8° 20' | +6.2 | | | | | | | | | |
| | 5° 45' | +8.6 | 8° 30' | +6.1 | | | | | | | | | |
| | 5° 50' | +8.5 | 8° 40' | +6.0 | | | | | | | | | |
| | 5° 55' | +8.4 | 8° 50' | +5.9 | | | | | | | | | |
| | 6° 0' | +8.3 | 9° 0' | +5.8 | | | | | | | | | |
| | 6° 5' | +8.2 | 9° 10' | +5.7 | | | | | | | | | |
| | 6° 10' | +8.1 | 9° 20' | +5.6 | | | | | | | | | |
| | 6° 15' | +8.0 | 9° 30' | +5.5 | | | | | | | | | |
| | 6° 20' | +7.9 | 9° 40' | +5.4 | | | | | | | | | |
| | 6° 25' | +7.8 | 9° 50' | +5.4 | | | | | | | | | |

Table 1

Combined Dip and Semidiameter

Table 1

These corrections change sextant altitudes to *Sa* and *Ma*, the apparent altitudes of the centers. For height of eye beyond the range of the table, combine the value in the zero column with dip from the *Nautical Almanac* correction table.






| | | Height of Eye in Feet | | | | | | | | | | |
|---|--|---------------------------------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|
| | | 0 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| Sun | Upper Limb  | April-Sept. -15.9 Oct.-March -16.2 | -17.6 -17.8 | -17.8 -18.1 | -18.1 -18.3 | -18.3 -18.5 | -18.5 -18.7 | -18.6 -18.9 | -18.8 -19.1 | -19.0 -19.2 | -19.1 -19.4 | -19.3 -19.5 |
| | Lower Limb  | April-Sept. +15.9 Oct.-March +16.2 | +14.2 +14.5 | +13.9 +14.2 | +13.7 +14.0 | +13.5 +13.8 | +13.3 +13.6 | +13.1 +13.4 | +13.0 +13.2 | +12.8 +13.1 | +12.7 +12.9 | +12.5 +12.8 |
| Star or Planet |  | 0.0 | -1.7 | -1.9 | -2.2 | -2.4 | -2.6 | -2.7 | -2.9 | -3.1 | -3.2 | -3.4 |
| Moon's Upper Limb  | | H.P. | | | | | | | | | | |
| | 54.0 | -14.7 | -16.4 | -16.7 | -16.9 | -17.1 | -17.3 | -17.5 | -17.6 | -17.8 | -17.9 | -18.1 |
| | .5 | -14.9 | -16.5 | -16.8 | -17.0 | -17.2 | -17.4 | -17.6 | -17.8 | -17.9 | -18.1 | -18.2 |
| | 55.0 | -15.0 | -16.7 | -16.9 | -17.2 | -17.4 | -17.6 | -17.7 | -17.9 | -18.1 | -18.2 | -18.4 |
| | .5 | -15.1 | -16.8 | -17.1 | -17.3 | -17.5 | -17.7 | -17.9 | -18.0 | -18.2 | -18.3 | -18.5 |
| | 56.0 | -15.3 | -16.9 | -17.2 | -17.4 | -17.6 | -17.8 | -18.0 | -18.2 | -18.3 | -18.5 | -18.6 |
| | .5 | -15.4 | -17.1 | -17.3 | -17.6 | -17.8 | -18.0 | -18.1 | -18.3 | -18.5 | -18.6 | -18.8 |
| | 57.0 | -15.5 | -17.2 | -17.5 | -17.7 | -17.9 | -18.1 | -18.3 | -18.4 | -18.6 | -18.8 | -18.9 |
| | .5 | -15.7 | -17.4 | -17.6 | -17.8 | -18.0 | -18.2 | -18.4 | -18.6 | -18.7 | -18.9 | -19.0 |
| | 58.0 | -15.8 | -17.5 | -17.7 | -18.0 | -18.2 | -18.4 | -18.6 | -18.7 | -18.9 | -19.0 | -19.2 |
| | .5 | -15.9 | -17.6 | -17.9 | -18.1 | -18.3 | -18.5 | -18.7 | -18.9 | -19.0 | -19.2 | -19.3 |
| | 59.0 | -16.1 | -17.8 | -18.0 | -18.3 | -18.5 | -18.6 | -18.8 | -19.0 | -19.2 | -19.3 | -19.4 |
| | .5 | -16.2 | -17.9 | -18.2 | -18.4 | -18.6 | -18.8 | -19.0 | -19.1 | -19.3 | -19.4 | -19.6 |
| | 60.0 | -16.4 | -18.0 | -18.3 | -18.5 | -18.7 | -18.9 | -19.1 | -19.3 | -19.4 | -19.6 | -19.7 |
| | .5 | -16.5 | -18.2 | -18.4 | -18.7 | -18.9 | -19.1 | -19.2 | -19.4 | -19.6 | -19.7 | -19.9 |
| | 61.0 | -16.6 | -18.3 | -18.6 | -18.8 | -19.0 | -19.2 | -19.4 | -19.5 | -19.7 | -19.8 | -20.0 |
| | .5 | -16.8 | -18.4 | -18.7 | -18.9 | -19.1 | -19.3 | -19.5 | -19.7 | -19.8 | -20.0 | -20.1 |
| Moon's Lower Limb  | | H.P. | | | | | | | | | | |
| | 54.0 | +14.7 | +13.0 | +12.8 | +12.5 | +12.3 | +12.1 | +12.0 | +11.8 | +11.6 | +11.5 | +11.3 |
| | .5 | +14.9 | +13.2 | +12.9 | +12.7 | +12.5 | +12.3 | +12.1 | +11.9 | +11.8 | +11.6 | +11.5 |
| | 55.0 | +15.0 | +13.3 | +13.0 | +12.8 | +12.6 | +12.4 | +12.2 | +12.1 | +11.9 | +11.8 | +11.6 |
| | .5 | +15.1 | +13.4 | +13.2 | +13.0 | +12.7 | +12.6 | +12.4 | +12.2 | +12.1 | +11.9 | +11.8 |
| | 56.0 | +15.3 | +13.6 | +13.3 | +13.1 | +12.9 | +12.7 | +12.5 | +12.3 | +12.2 | +12.0 | +11.9 |
| | .5 | +15.4 | +13.7 | +13.5 | +13.2 | +13.0 | +12.8 | +12.6 | +12.5 | +12.3 | +12.2 | +12.0 |
| | 57.0 | +15.5 | +13.8 | +13.6 | +13.4 | +13.2 | +13.0 | +12.8 | +12.6 | +12.5 | +12.3 | +12.2 |
| | .5 | +15.7 | +14.0 | +13.7 | +13.5 | +13.3 | +13.1 | +12.9 | +12.8 | +12.6 | +12.4 | +12.3 |
| | 58.0 | +15.8 | +14.1 | +13.9 | +13.6 | +13.4 | +13.2 | +13.1 | +12.9 | +12.7 | +12.6 | +12.4 |
| | .5 | +15.9 | +14.3 | +14.0 | +13.8 | +13.6 | +13.4 | +13.2 | +13.0 | +12.9 | +12.7 | +12.6 |
| | 59.0 | +16.1 | +14.4 | +14.1 | +13.9 | +13.7 | +13.5 | +13.3 | +13.2 | +13.0 | +12.9 | +12.7 |
| | .5 | +16.2 | +14.5 | +14.3 | +14.0 | +13.8 | +13.6 | +13.5 | +13.3 | +13.1 | +13.0 | +12.8 |
| | 60.0 | +16.4 | +14.7 | +14.4 | +14.2 | +14.0 | +13.8 | +13.6 | +13.4 | +13.3 | +13.1 | +13.0 |
| | .5 | +16.5 | +14.8 | +14.5 | +14.3 | +14.1 | +13.9 | +13.7 | +13.6 | +13.4 | +13.3 | +13.1 |
| | 61.0 | +16.6 | +14.9 | +14.7 | +14.4 | +14.2 | +14.1 | +13.9 | +13.7 | +13.5 | +13.4 | +13.3 |
| | .5 | +16.8 | +15.1 | +14.8 | +14.6 | +14.4 | +14.2 | +14.0 | +13.8 | +13.7 | +13.5 | +13.4 |

Table 2

| Ma | H.P.= 53' | | H.P.= 55' | | H.P.= 57' | | H.P.= 59' | | H.P.= 61' | |
|-------|-----------|------|-----------|------|-----------|------|-----------|------|-----------|------|
| | r&p | Q | r&p | Q | r&p | Q | r&p | Q | r&p | Q |
| 4° 0' | 41.14 | 27.3 | 43.13 | 29.3 | 45.13 | 31.4 | 47.12 | 33.5 | 49.12 | 35.6 |
| 2' | 41.21 | 27.6 | 43.20 | 29.7 | 45.20 | 31.8 | 47.19 | 34.0 | 49.19 | 36.1 |
| 4' | 41.28 | 28.0 | 43.27 | 30.1 | 45.27 | 32.2 | 47.26 | 34.4 | 49.26 | 36.5 |
| 6' | 41.35 | 28.4 | 43.34 | 30.5 | 45.34 | 32.7 | 47.33 | 34.8 | 49.33 | 37.0 |
| 8' | 41.41 | 28.8 | 43.41 | 30.9 | 45.41 | 33.1 | 47.40 | 35.2 | 49.40 | 37.4 |
| 10' | 41.48 | 29.2 | 43.48 | 31.3 | 45.47 | 33.5 | 47.47 | 35.7 | 49.46 | 37.8 |
| 12' | 41.55 | 29.5 | 43.54 | 31.7 | 45.54 | 33.9 | 47.53 | 36.1 | 49.53 | 38.3 |
| 14' | 41.62 | 29.9 | 43.61 | 32.1 | 45.61 | 34.3 | 47.60 | 36.5 | 49.60 | 38.7 |
| 16' | 41.68 | 30.3 | 43.68 | 32.5 | 45.67 | 34.7 | 47.67 | 36.9 | 49.66 | 39.2 |
| 18' | 41.74 | 30.7 | 43.74 | 32.9 | 45.73 | 35.1 | 47.73 | 37.3 | 49.72 | 39.6 |
| 20' | 41.81 | 31.1 | 43.80 | 33.3 | 45.80 | 35.5 | 47.79 | 37.8 | 49.79 | 40.0 |
| 22' | 41.87 | 31.4 | 43.87 | 33.7 | 45.86 | 35.9 | 47.86 | 38.2 | 49.85 | 40.5 |
| 24' | 41.93 | 31.8 | 43.93 | 34.1 | 45.92 | 36.3 | 47.92 | 38.6 | 49.91 | 40.9 |
| 26' | 42.00 | 32.2 | 43.99 | 34.5 | 45.98 | 36.8 | 47.98 | 39.1 | 49.97 | 41.4 |
| 28' | 42.06 | 32.6 | 44.05 | 34.9 | 46.05 | 37.2 | 48.04 | 39.5 | 50.03 | 41.8 |
| 30' | 42.12 | 33.0 | 44.11 | 35.3 | 46.11 | 37.6 | 48.10 | 39.9 | 50.09 | 42.2 |
| 32' | 42.18 | 33.3 | 44.17 | 35.7 | 46.16 | 38.0 | 48.16 | 40.3 | 50.15 | 42.7 |
| 34' | 42.24 | 33.7 | 44.23 | 36.0 | 46.22 | 38.4 | 48.22 | 40.8 | 50.21 | 43.1 |
| 36' | 42.29 | 34.1 | 44.29 | 36.4 | 46.28 | 38.8 | 48.28 | 41.2 | 50.27 | 43.6 |
| 38' | 42.35 | 34.5 | 44.34 | 36.8 | 46.34 | 39.2 | 48.33 | 41.6 | 50.33 | 44.0 |
| 40' | 42.41 | 34.9 | 44.40 | 37.2 | 46.40 | 39.6 | 48.39 | 42.0 | 50.38 | 44.5 |
| 42' | 42.46 | 35.2 | 44.46 | 37.6 | 46.45 | 40.0 | 48.45 | 42.5 | 50.44 | 44.9 |
| 44' | 42.52 | 35.6 | 44.51 | 38.0 | 46.51 | 40.5 | 48.50 | 42.9 | 50.49 | 45.3 |
| 46' | 42.58 | 36.0 | 44.57 | 38.4 | 46.56 | 40.9 | 48.56 | 43.3 | 50.55 | 45.8 |
| 48' | 42.63 | 36.4 | 44.62 | 38.8 | 46.62 | 41.3 | 48.61 | 43.7 | 50.60 | 46.2 |
| 50' | 42.68 | 36.8 | 44.68 | 39.2 | 46.67 | 41.7 | 48.66 | 44.2 | 50.66 | 46.7 |
| 52' | 42.74 | 37.2 | 44.73 | 39.6 | 46.72 | 42.1 | 48.72 | 44.6 | 50.71 | 47.1 |
| 54' | 42.79 | 37.5 | 44.78 | 40.0 | 46.78 | 42.5 | 48.77 | 45.0 | 50.76 | 47.6 |
| 56' | 42.84 | 37.9 | 44.84 | 40.4 | 46.83 | 42.9 | 48.82 | 45.5 | 50.81 | 48.0 |
| 58' | 42.89 | 38.3 | 44.89 | 40.8 | 46.88 | 43.3 | 48.87 | 45.9 | 50.87 | 48.4 |
| ----- | | | | | | | | | | |
| 5° 0' | 42.94 | 38.7 | 44.94 | 41.2 | 46.93 | 43.8 | 48.92 | 46.3 | 50.92 | 48.9 |
| 2' | 43.00 | 39.1 | 44.99 | 41.6 | 46.98 | 44.2 | 48.97 | 46.7 | 50.97 | 49.3 |
| 4' | 43.05 | 39.4 | 45.04 | 42.0 | 47.03 | 44.6 | 49.02 | 47.2 | 51.02 | 49.8 |
| 6' | 43.09 | 39.8 | 45.09 | 42.4 | 47.08 | 45.0 | 49.07 | 47.6 | 51.07 | 50.2 |
| 8' | 43.14 | 40.2 | 45.14 | 42.8 | 47.13 | 45.4 | 49.12 | 48.0 | 51.11 | 50.7 |
| 10' | 43.19 | 40.6 | 45.18 | 43.2 | 47.18 | 45.8 | 49.17 | 48.4 | 51.16 | 51.1 |
| 12' | 43.24 | 41.0 | 45.23 | 43.6 | 47.22 | 46.2 | 49.22 | 48.9 | 51.21 | 51.5 |
| 14' | 43.29 | 41.4 | 45.28 | 44.0 | 47.27 | 46.6 | 49.26 | 49.3 | 51.26 | 52.0 |
| 16' | 43.33 | 41.7 | 45.33 | 44.4 | 47.32 | 47.1 | 49.31 | 49.7 | 51.30 | 52.4 |
| 18' | 43.38 | 42.1 | 45.37 | 44.8 | 47.36 | 47.5 | 49.36 | 50.2 | 51.35 | 52.9 |
| 20' | 43.43 | 42.5 | 45.42 | 45.2 | 47.41 | 47.9 | 49.40 | 50.6 | 51.39 | 53.3 |
| 22' | 43.47 | 42.9 | 45.46 | 45.6 | 47.46 | 48.3 | 49.45 | 51.0 | 51.44 | 53.8 |
| 24' | 43.52 | 43.3 | 45.51 | 46.0 | 47.50 | 48.7 | 49.49 | 51.4 | 51.48 | 54.2 |
| 26' | 43.56 | 43.7 | 45.55 | 46.4 | 47.55 | 49.1 | 49.54 | 51.9 | 51.53 | 54.6 |
| 28' | 43.61 | 44.0 | 45.60 | 46.8 | 47.59 | 49.5 | 49.58 | 52.3 | 51.57 | 55.1 |
| 30' | 43.65 | 44.4 | 45.64 | 47.2 | 47.63 | 50.0 | 49.62 | 52.7 | 51.61 | 55.5 |
| 32' | 43.69 | 44.8 | 45.68 | 47.6 | 47.68 | 50.4 | 49.67 | 53.2 | 51.66 | 56.0 |
| 34' | 43.74 | 45.2 | 45.73 | 48.0 | 47.72 | 50.8 | 49.71 | 53.6 | 51.70 | 56.4 |
| 36' | 43.78 | 45.6 | 45.77 | 48.4 | 47.76 | 51.2 | 49.75 | 54.0 | 51.74 | 56.9 |
| 38' | 43.82 | 46.0 | 45.81 | 48.8 | 47.80 | 51.6 | 49.79 | 54.5 | 51.78 | 57.3 |
| 40' | 43.86 | 46.4 | 45.85 | 49.2 | 47.84 | 52.0 | 49.83 | 54.9 | 51.82 | 57.8 |
| 42' | 43.90 | 46.7 | 45.89 | 49.6 | 47.88 | 52.4 | 49.87 | 55.3 | 51.86 | 58.2 |
| 44' | 43.94 | 47.1 | 45.93 | 50.0 | 47.92 | 52.9 | 49.91 | 55.7 | 51.90 | 58.6 |
| 46' | 43.98 | 47.5 | 45.97 | 50.4 | 47.96 | 53.3 | 49.95 | 56.2 | 51.94 | 59.1 |
| 48' | 44.02 | 47.9 | 46.01 | 50.8 | 48.00 | 53.7 | 49.99 | 56.6 | 51.98 | 59.5 |
| 50' | 44.06 | 48.3 | 46.05 | 51.2 | 48.04 | 54.1 | 50.03 | 57.0 | 52.02 | 60.0 |
| 52' | 44.10 | 48.7 | 46.09 | 51.6 | 48.08 | 54.5 | 50.07 | 57.5 | 52.06 | 60.4 |
| 54' | 44.14 | 49.0 | 46.13 | 52.0 | 48.12 | 54.9 | 50.11 | 57.9 | 52.10 | 60.9 |
| 56' | 44.18 | 49.4 | 46.17 | 52.4 | 48.16 | 55.3 | 50.15 | 58.3 | 52.14 | 61.3 |
| 58' | 44.22 | 49.8 | 46.21 | 52.8 | 48.20 | 55.8 | 50.18 | 58.7 | 52.17 | 61.8 |

Table 2

| for H.P. increments | | |
|---------------------|------|-----|
| extra H.P. | r&p | Q |
| 0.1 | 0.10 | 0.1 |
| 0.2 | 0.20 | 0.2 |
| 0.3 | 0.30 | 0.3 |
| 0.4 | 0.40 | 0.5 |
| 0.5 | 0.50 | 0.6 |
| 0.6 | 0.60 | 0.7 |
| 0.7 | 0.70 | 0.8 |
| 0.8 | 0.80 | 0.9 |
| 0.9 | 0.90 | 1.0 |
| 1.0 | 1.00 | 1.2 |
| 1.1 | 1.10 | 1.3 |
| 1.2 | 1.20 | 1.4 |
| 1.3 | 1.30 | 1.5 |
| 1.4 | 1.40 | 1.6 |
| 1.5 | 1.50 | 1.7 |
| 1.6 | 1.60 | 1.9 |
| 1.7 | 1.70 | 2.0 |
| 1.8 | 1.79 | 2.1 |
| 1.9 | 1.89 | 2.2 |

| for H.P. increments | | |
|---------------------|------|-----|
| extra H.P. | r&p | Q |
| 0.1 | 0.10 | 0.1 |
| 0.2 | 0.20 | 0.3 |
| 0.3 | 0.30 | 0.4 |
| 0.4 | 0.40 | 0.6 |
| 0.5 | 0.50 | 0.7 |
| 0.6 | 0.60 | 0.8 |
| 0.7 | 0.70 | 1.0 |
| 0.8 | 0.80 | 1.1 |
| 0.9 | 0.90 | 1.2 |
| 1.0 | 1.00 | 1.4 |
| 1.1 | 1.10 | 1.5 |
| 1.2 | 1.19 | 1.7 |
| 1.3 | 1.29 | 1.8 |
| 1.4 | 1.39 | 1.9 |
| 1.5 | 1.49 | 2.1 |
| 1.6 | 1.59 | 2.2 |
| 1.7 | 1.69 | 2.4 |
| 1.8 | 1.79 | 2.5 |
| 1.9 | 1.89 | 2.6 |

Table 3

Table 3

| Sa | for SUN | | SATURN, JUPITER or STAR | | For VENUS or MARS, check bottom of page 259 in <i>Nautical Almanac</i> for a value of "p". If none is given, use Star column. | | | | | | | | | | 4° |
|-------|---------|-----|-------------------------------|-----|---|-----|---------|-----|---------|-----|---------|-----|---------|-----|----|
| | r&p | Q | r&p | Q | p = 0.1 | | p = 0.2 | | p = 0.3 | | p = 0.4 | | p = 0.5 | | |
| | | | | | r&p | Q | r&p | Q | r&p | Q | r&p | Q | r&p | Q | |
| 0' | 11:60 | 2.2 | 11:75 | 2.1 | 11:65 | 2.2 | 11:55 | 2.2 | 11:45 | 2.3 | 11:35 | 2.4 | 11:25 | 2.5 | |
| 2' | 11:53 | 2.2 | 11:67 | 2.1 | 11:57 | 2.1 | 11:47 | 2.2 | 11:37 | 2.3 | 11:27 | 2.4 | 11:17 | 2.5 | |
| 4' | 11:45 | 2.2 | 11:60 | 2.0 | 11:50 | 2.1 | 11:40 | 2.2 | 11:30 | 2.3 | 11:20 | 2.4 | 11:10 | 2.5 | |
| 6' | 11:38 | 2.1 | 11:53 | 2.0 | 11:43 | 2.1 | 11:33 | 2.2 | 11:23 | 2.3 | 11:13 | 2.3 | 11:03 | 2.4 | |
| 8' | 11:31 | 2.1 | 11:46 | 2.0 | 11:36 | 2.1 | 11:26 | 2.2 | 11:16 | 2.2 | 11:06 | 2.3 | 10:96 | 2.4 | |
| 10' | 11:24 | 2.1 | 11:39 | 2.0 | 11:29 | 2.0 | 11:19 | 2.1 | 11:09 | 2.2 | 10:99 | 2.3 | 10:89 | 2.4 | |
| 12' | 11:17 | 2.1 | 11:32 | 1.9 | 11:22 | 2.0 | 11:12 | 2.1 | 11:02 | 2.2 | 10:92 | 2.3 | 10:82 | 2.4 | |
| 14' | 11:11 | 2.0 | 11:25 | 1.9 | 11:15 | 2.0 | 11:05 | 2.1 | 10:95 | 2.2 | 10:85 | 2.3 | 10:75 | 2.4 | |
| 16' | 11:04 | 2.0 | 11:19 | 1.9 | 11:09 | 2.0 | 10:99 | 2.1 | 10:89 | 2.2 | 10:79 | 2.2 | 10:69 | 2.3 | |
| 18' | 10:97 | 2.0 | 11:12 | 1.9 | 11:02 | 2.0 | 10:92 | 2.0 | 10:82 | 2.1 | 10:72 | 2.2 | 10:62 | 2.3 | |
| 20' | 10:91 | 2.0 | 11:05 | 1.8 | 10:95 | 1.9 | 10:85 | 2.0 | 10:75 | 2.1 | 10:65 | 2.2 | 10:55 | 2.3 | |
| 22' | 10:84 | 2.0 | 10:99 | 1.8 | 10:89 | 1.9 | 10:79 | 2.0 | 10:69 | 2.1 | 10:59 | 2.2 | 10:49 | 2.3 | |
| 24' | 10:78 | 1.9 | 10:92 | 1.8 | 10:82 | 1.9 | 10:72 | 2.0 | 10:62 | 2.1 | 10:52 | 2.2 | 10:42 | 2.3 | |
| 26' | 10:71 | 1.9 | 10:86 | 1.8 | 10:76 | 1.9 | 10:66 | 2.0 | 10:56 | 2.1 | 10:46 | 2.2 | 10:36 | 2.3 | |
| 28' | 10:65 | 1.9 | 10:80 | 1.8 | 10:70 | 1.9 | 10:60 | 2.0 | 10:50 | 2.0 | 10:40 | 2.1 | 10:30 | 2.2 | |
| 30' | 10:59 | 1.9 | 10:73 | 1.7 | 10:63 | 1.8 | 10:53 | 1.9 | 10:43 | 2.0 | 10:33 | 2.1 | 10:23 | 2.2 | |
| 32' | 10:52 | 1.9 | 10:67 | 1.7 | 10:57 | 1.8 | 10:47 | 1.9 | 10:37 | 2.0 | 10:27 | 2.1 | 10:17 | 2.2 | |
| 34' | 10:46 | 1.8 | 10:61 | 1.7 | 10:51 | 1.8 | 10:41 | 1.9 | 10:31 | 2.0 | 10:21 | 2.1 | 10:11 | 2.2 | |
| 36' | 10:40 | 1.8 | 10:55 | 1.7 | 10:45 | 1.8 | 10:35 | 1.9 | 10:25 | 2.0 | 10:15 | 2.1 | 10:05 | 2.2 | |
| 38' | 10:34 | 1.8 | 10:49 | 1.7 | 10:39 | 1.8 | 10:29 | 1.9 | 10:19 | 2.0 | 10:09 | 2.1 | 9:99 | 2.2 | |
| 40' | 10:28 | 1.8 | 10:43 | 1.6 | 10:33 | 1.7 | 10:23 | 1.8 | 10:13 | 1.9 | 10:03 | 2.0 | 9:93 | 2.1 | |
| 42' | 10:22 | 1.8 | 10:37 | 1.6 | 10:27 | 1.7 | 10:17 | 1.8 | 10:07 | 1.9 | 9:97 | 2.0 | 9:87 | 2.1 | |
| 44' | 10:17 | 1.8 | 10:31 | 1.6 | 10:21 | 1.7 | 10:11 | 1.8 | 10:01 | 1.9 | 9:91 | 2.0 | 9:81 | 2.1 | |
| 46' | 10:11 | 1.7 | 10:25 | 1.6 | 10:15 | 1.7 | 10:06 | 1.8 | 9:96 | 1.9 | 9:86 | 2.0 | 9:76 | 2.1 | |
| 48' | 10:05 | 1.7 | 10:20 | 1.6 | 10:10 | 1.7 | 10:00 | 1.8 | 9:90 | 1.9 | 9:80 | 2.0 | 9:70 | 2.1 | |
| 50' | 9:99 | 1.7 | 10:14 | 1.6 | 10:04 | 1.7 | 9:94 | 1.8 | 9:84 | 1.9 | 9:74 | 2.0 | 9:64 | 2.1 | |
| 52' | 9:94 | 1.7 | 10:08 | 1.5 | 9:99 | 1.6 | 9:89 | 1.7 | 9:79 | 1.9 | 9:69 | 2.0 | 9:59 | 2.1 | |
| 54' | 9:88 | 1.7 | 10:03 | 1.5 | 9:93 | 1.6 | 9:83 | 1.7 | 9:73 | 1.8 | 9:63 | 1.9 | 9:53 | 2.0 | |
| 56' | 9:83 | 1.7 | 9:97 | 1.5 | 9:88 | 1.6 | 9:78 | 1.7 | 9:68 | 1.8 | 9:58 | 1.9 | 9:48 | 2.0 | |
| 58' | 9:77 | 1.6 | 9:92 | 1.5 | 9:82 | 1.6 | 9:72 | 1.7 | 9:62 | 1.8 | 9:52 | 1.9 | 9:42 | 2.0 | |
| 5° 0' | 9:72 | 1.6 | 9:87 | 1.5 | 9:77 | 1.6 | 9:67 | 1.7 | 9:57 | 1.8 | 9:47 | 1.9 | 9:37 | 2.0 | |
| 2' | 9:67 | 1.6 | 9:81 | 1.5 | 9:71 | 1.6 | 9:61 | 1.7 | 9:51 | 1.8 | 9:41 | 1.9 | 9:32 | 2.0 | |
| 4' | 9:61 | 1.6 | 9:76 | 1.4 | 9:66 | 1.6 | 9:56 | 1.7 | 9:46 | 1.8 | 9:36 | 1.9 | 9:26 | 2.0 | |
| 6' | 9:56 | 1.6 | 9:71 | 1.4 | 9:61 | 1.5 | 9:51 | 1.6 | 9:41 | 1.8 | 9:31 | 1.9 | 9:21 | 2.0 | |
| 8' | 9:51 | 1.6 | 9:66 | 1.4 | 9:56 | 1.5 | 9:46 | 1.6 | 9:36 | 1.7 | 9:26 | 1.9 | 9:16 | 2.0 | |
| 10' | 9:46 | 1.6 | 9:61 | 1.4 | 9:51 | 1.5 | 9:41 | 1.6 | 9:31 | 1.7 | 9:21 | 1.8 | 9:11 | 2.0 | |
| 12' | 9:41 | 1.5 | 9:55 | 1.4 | 9:46 | 1.5 | 9:36 | 1.6 | 9:26 | 1.7 | 9:16 | 1.8 | 9:06 | 1.9 | |
| 14' | 9:36 | 1.5 | 9:50 | 1.4 | 9:41 | 1.5 | 9:31 | 1.6 | 9:21 | 1.7 | 9:11 | 1.8 | 9:01 | 1.9 | |
| 16' | 9:31 | 1.5 | 9:45 | 1.4 | 9:36 | 1.5 | 9:26 | 1.6 | 9:16 | 1.7 | 9:06 | 1.8 | 8:96 | 1.9 | |
| 18' | 9:26 | 1.5 | 9:41 | 1.3 | 9:31 | 1.5 | 9:21 | 1.6 | 9:11 | 1.7 | 9:01 | 1.8 | 8:91 | 1.9 | |
| 20' | 9:21 | 1.5 | 9:36 | 1.3 | 9:26 | 1.4 | 9:16 | 1.6 | 9:06 | 1.7 | 8:96 | 1.8 | 8:86 | 1.9 | |
| 22' | 9:16 | 1.5 | 9:31 | 1.3 | 9:21 | 1.4 | 9:11 | 1.5 | 9:01 | 1.7 | 8:91 | 1.8 | 8:81 | 1.9 | |
| 24' | 9:11 | 1.5 | 9:26 | 1.3 | 9:16 | 1.4 | 9:06 | 1.5 | 8:96 | 1.6 | 8:86 | 1.8 | 8:76 | 1.9 | |
| 26' | 9:07 | 1.5 | 9:21 | 1.3 | 9:11 | 1.4 | 9:01 | 1.5 | 8:91 | 1.6 | 8:81 | 1.8 | 8:72 | 1.9 | |
| 28' | 9:02 | 1.4 | 9:17 | 1.3 | 9:07 | 1.4 | 8:97 | 1.5 | 8:87 | 1.6 | 8:77 | 1.7 | 8:67 | 1.9 | |
| 5° 0' | 9:72 | 1.6 | 9:87 | 1.5 | 9:77 | 1.6 | 9:67 | 1.7 | 9:57 | 1.8 | 9:47 | 1.9 | 9:37 | 2.0 | |
| 2' | 9:67 | 1.6 | 9:81 | 1.5 | 9:71 | 1.6 | 9:61 | 1.7 | 9:51 | 1.8 | 9:41 | 1.9 | 9:32 | 2.0 | |
| 4' | 9:61 | 1.6 | 9:76 | 1.4 | 9:66 | 1.6 | 9:56 | 1.7 | 9:46 | 1.8 | 9:36 | 1.9 | 9:26 | 2.0 | |
| 6' | 9:56 | 1.6 | 9:71 | 1.4 | 9:61 | 1.5 | 9:51 | 1.6 | 9:41 | 1.8 | 9:31 | 1.9 | 9:21 | 2.0 | |
| 8' | 9:51 | 1.6 | 9:66 | 1.4 | 9:56 | 1.5 | 9:46 | 1.6 | 9:36 | 1.7 | 9:26 | 1.9 | 9:16 | 2.0 | |
| 10' | 9:46 | 1.6 | 9:61 | 1.4 | 9:51 | 1.5 | 9:41 | 1.6 | 9:31 | 1.7 | 9:21 | 1.8 | 9:11 | 2.0 | |
| 12' | 9:41 | 1.5 | 9:55 | 1.4 | 9:46 | 1.5 | 9:36 | 1.6 | 9:26 | 1.7 | 9:16 | 1.8 | 9:06 | 1.9 | |
| 14' | 9:36 | 1.5 | 9:50 | 1.4 | 9:41 | 1.5 | 9:31 | 1.6 | 9:21 | 1.7 | 9:11 | 1.8 | 9:01 | 1.9 | |
| 16' | 9:31 | 1.5 | 9:45 | 1.4 | 9:36 | 1.5 | 9:26 | 1.6 | 9:16 | 1.7 | 9:06 | 1.8 | 8:96 | 1.9 | |
| 18' | 9:26 | 1.5 | 9:41 | 1.3 | 9:31 | 1.5 | 9:21 | 1.6 | 9:11 | 1.7 | 9:01 | 1.8 | 8:91 | 1.9 | |
| 20' | 9:21 | 1.5 | 9:36 | 1.3 | 9:26 | 1.4 | 9:16 | 1.6 | 9:06 | 1.7 | 8:96 | 1.8 | 8:86 | 1.9 | |
| 22' | 9:16 | 1.5 | 9:31 | 1.3 | 9:21 | 1.4 | 9:11 | 1.5 | 9:01 | 1.7 | 8:91 | 1.8 | 8:81 | 1.9 | |
| 24' | 9:11 | 1.5 | 9:26 | 1.3 | 9:16 | 1.4 | 9:06 | 1.5 | 8:96 | 1.6 | 8:86 | 1.8 | 8:76 | 1.9 | |
| 26' | 9:07 | 1.5 | 9:21 | 1.3 | 9:11 | 1.4 | 9:01 | 1.5 | 8:91 | 1.6 | 8:81 | 1.8 | 8:72 | 1.9 | |
| 28' | 9:02 | 1.4 | 9:17 | 1.3 | 9:07 | 1.4 | 8:97 | 1.5 | 8:87 | 1.6 | 8:77 | 1.7 | 8:67 | 1.9 | |

Table 4

Table 4

| | | Ma | | | | | | | | | |
|-------------|-----------|-------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | 5° | 10° | 15° | 20° | 25° | 30° | 40° | 50° | 60° | 90° |
| H.P. | | Moon's Augmented Semidiameter | | | | | | | | | |
| 53.9 | | 14.'71 | 14.'73 | 14.'75 | 14.'77 | 14.'79 | 14.'80 | 14.'84 | 14.'87 | 14.'89 | 14.'92 |
| 54.0 | | 14.'74 | 14.'76 | 14.'78 | 14.'79 | 14.'81 | 14.'83 | 14.'87 | 14.'89 | 14.'92 | 14.'95 |
| | .1 | 14.'76 | 14.'78 | 14.'80 | 14.'82 | 14.'84 | 14.'86 | 14.'89 | 14.'92 | 14.'95 | 14.'98 |
| | .2 | 14.'79 | 14.'81 | 14.'83 | 14.'85 | 14.'87 | 14.'89 | 14.'92 | 14.'95 | 14.'97 | 15.'01 |
| | .3 | 14.'82 | 14.'84 | 14.'86 | 14.'88 | 14.'90 | 14.'91 | 14.'95 | 14.'98 | 15.'00 | 15.'03 |
| | .4 | 14.'84 | 14.'86 | 14.'88 | 14.'90 | 14.'92 | 14.'94 | 14.'98 | 15.'01 | 15.'03 | 15.'06 |
| | .5 | 14.'87 | 14.'89 | 14.'91 | 14.'93 | 14.'95 | 14.'97 | 15.'00 | 15.'03 | 15.'06 | 15.'09 |
| | .6 | 14.'90 | 14.'92 | 14.'94 | 14.'96 | 14.'98 | 15.'00 | 15.'03 | 15.'06 | 15.'09 | 15.'12 |
| | .7 | 14.'93 | 14.'95 | 14.'97 | 14.'99 | 15.'01 | 15.'03 | 15.'06 | 15.'09 | 15.'11 | 15.'15 |
| | .8 | 14.'95 | 14.'97 | 14.'99 | 15.'01 | 15.'03 | 15.'05 | 15.'09 | 15.'12 | 15.'14 | 15.'17 |
| | .9 | 14.'98 | 15.'00 | 15.'02 | 15.'04 | 15.'06 | 15.'08 | 15.'12 | 15.'15 | 15.'17 | 15.'20 |
| 55.0 | | 15.'01 | 15.'03 | 15.'05 | 15.'07 | 15.'09 | 15.'11 | 15.'14 | 15.'17 | 15.'20 | 15.'23 |
| | .1 | 15.'04 | 15.'06 | 15.'08 | 15.'10 | 15.'12 | 15.'14 | 15.'17 | 15.'20 | 15.'23 | 15.'26 |
| | .2 | 15.'06 | 15.'08 | 15.'10 | 15.'13 | 15.'14 | 15.'16 | 15.'20 | 15.'23 | 15.'25 | 15.'29 |
| | .3 | 15.'09 | 15.'11 | 15.'13 | 15.'15 | 15.'17 | 15.'19 | 15.'23 | 15.'26 | 15.'28 | 15.'32 |
| | .4 | 15.'12 | 15.'14 | 15.'16 | 15.'18 | 15.'20 | 15.'22 | 15.'25 | 15.'29 | 15.'31 | 15.'34 |
| | .5 | 15.'15 | 15.'17 | 15.'19 | 15.'21 | 15.'23 | 15.'25 | 15.'28 | 15.'31 | 15.'34 | 15.'37 |
| | .6 | 15.'17 | 15.'19 | 15.'21 | 15.'24 | 15.'26 | 15.'27 | 15.'31 | 15.'34 | 15.'37 | 15.'40 |
| | .7 | 15.'20 | 15.'22 | 15.'24 | 15.'26 | 15.'28 | 15.'30 | 15.'34 | 15.'37 | 15.'39 | 15.'43 |
| | .8 | 15.'23 | 15.'25 | 15.'27 | 15.'29 | 15.'31 | 15.'33 | 15.'37 | 15.'40 | 15.'42 | 15.'46 |
| | .9 | 15.'25 | 15.'28 | 15.'30 | 15.'32 | 15.'34 | 15.'36 | 15.'39 | 15.'42 | 15.'45 | 15.'48 |
| 56.0 | | 15.'28 | 15.'30 | 15.'32 | 15.'35 | 15.'37 | 15.'39 | 15.'42 | 15.'45 | 15.'48 | 15.'51 |
| | .1 | 15.'31 | 15.'33 | 15.'35 | 15.'37 | 15.'39 | 15.'41 | 15.'45 | 15.'48 | 15.'51 | 15.'54 |
| | .2 | 15.'34 | 15.'36 | 15.'38 | 15.'40 | 15.'42 | 15.'44 | 15.'48 | 15.'51 | 15.'53 | 15.'57 |
| | .3 | 15.'36 | 15.'39 | 15.'41 | 15.'43 | 15.'45 | 15.'47 | 15.'50 | 15.'54 | 15.'56 | 15.'60 |
| | .4 | 15.'39 | 15.'41 | 15.'43 | 15.'46 | 15.'48 | 15.'50 | 15.'53 | 15.'56 | 15.'59 | 15.'63 |
| | .5 | 15.'42 | 15.'44 | 15.'46 | 15.'48 | 15.'50 | 15.'52 | 15.'56 | 15.'59 | 15.'62 | 15.'65 |
| | .6 | 15.'45 | 15.'47 | 15.'49 | 15.'51 | 15.'53 | 15.'55 | 15.'59 | 15.'62 | 15.'65 | 15.'68 |
| | .7 | 15.'47 | 15.'50 | 15.'52 | 15.'54 | 15.'56 | 15.'58 | 15.'62 | 15.'65 | 15.'67 | 15.'71 |
| | .8 | 15.'50 | 15.'52 | 15.'54 | 15.'57 | 15.'59 | 15.'61 | 15.'64 | 15.'68 | 15.'70 | 15.'74 |
| | .9 | 15.'53 | 15.'55 | 15.'57 | 15.'59 | 15.'61 | 15.'63 | 15.'67 | 15.'70 | 15.'73 | 15.'77 |
| 57.0 | | 15.'55 | 15.'58 | 15.'60 | 15.'62 | 15.'64 | 15.'66 | 15.'70 | 15.'73 | 15.'76 | 15.'79 |
| | .1 | 15.'58 | 15.'60 | 15.'63 | 15.'65 | 15.'67 | 15.'69 | 15.'73 | 15.'76 | 15.'79 | 15.'82 |
| | .2 | 15.'61 | 15.'63 | 15.'65 | 15.'68 | 15.'70 | 15.'72 | 15.'76 | 15.'79 | 15.'81 | 15.'85 |
| | .3 | 15.'64 | 15.'66 | 15.'68 | 15.'70 | 15.'73 | 15.'75 | 15.'78 | 15.'82 | 15.'84 | 15.'88 |
| | .4 | 15.'66 | 15.'69 | 15.'71 | 15.'73 | 15.'75 | 15.'77 | 15.'81 | 15.'84 | 15.'87 | 15.'91 |
| | .5 | 15.'69 | 15.'71 | 15.'74 | 15.'76 | 15.'78 | 15.'80 | 15.'84 | 15.'87 | 15.'90 | 15.'94 |
| | .6 | 15.'72 | 15.'74 | 15.'76 | 15.'79 | 15.'81 | 15.'83 | 15.'87 | 15.'90 | 15.'93 | 15.'96 |
| | .7 | 15.'75 | 15.'77 | 15.'79 | 15.'81 | 15.'84 | 15.'86 | 15.'89 | 15.'93 | 15.'96 | 15.'99 |
| | .8 | 15.'77 | 15.'80 | 15.'82 | 15.'84 | 15.'86 | 15.'88 | 15.'92 | 15.'96 | 15.'98 | 16.'02 |
| | .9 | 15.'80 | 15.'82 | 15.'85 | 15.'87 | 15.'89 | 15.'91 | 15.'95 | 15.'98 | 16.'01 | 16.'05 |

Table 5

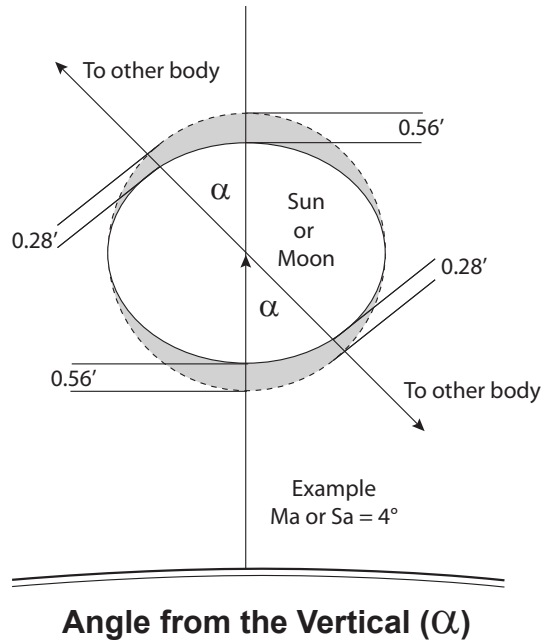
Table 5

SUN

| | day of the month | | | | | | |
|--------------|--------------------|-------|--------|--------|--------|--------|--------|
| | 1 | 5 | 10 | 15 | 20 | 25 | 30 |
| | sun's semidiameter | | | | | | |
| JAN. | 16.'29 | 16.29 | 16.'29 | 16.'29 | 16.'28 | 16.'27 | 16.'26 |
| FEB. | 16.'26 | 16.25 | 16.'23 | 16.'22 | 16.'20 | 16.'18 | |
| MAR. | 16.'17 | 16.15 | 16.'13 | 16.'11 | 16.'09 | 16.'06 | 16.'04 |
| APR. | 16.'03 | 16.01 | 15.'99 | 15.'97 | 15.'95 | 15.'92 | 15.'90 |
| MAY | 15.'90 | 15.88 | 15.'86 | 15.'85 | 15.'83 | 15.'82 | 15.'80 |
| JUNE | 15.'80 | 15.79 | 15.'78 | 15.'77 | 15.'77 | 15.'76 | 15.'76 |
| JULY | 15.'76 | 15.76 | 15.'76 | 15.'76 | 15.'77 | 15.'77 | 15.'78 |
| AUG. | 15.'78 | 15.79 | 15.'80 | 15.'82 | 15.'83 | 15.'85 | 15.'87 |
| SEPT. | 15.'87 | 15.89 | 15.'91 | 15.'93 | 15.'95 | 15.'97 | 16.'00 |
| OCT. | 16.'00 | 16.02 | 16.'04 | 16.'07 | 16.'09 | 16.'11 | 16.'13 |
| NOV. | 16.'14 | 16.16 | 16.'18 | 16.'20 | 16.'21 | 16.'23 | 16.'24 |
| DEC. | 16.'25 | 16.26 | 16.'27 | 16.'28 | 16.'28 | 16.'29 | 16.'29 |

Table 6

Table 6



| Ma or Sa | 0° | 10° | 15° | 20° | 25° | 30° | 35° | 40° | 45° | 50° | 55° | 60° | 70° | 80° |
|-----------------|-------------------------------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| | Apparent Reduction of Semidiameter: | | | | | | | | | | | | | |
| 4° 0' | 0.56 | 0.54 | 0.52 | 0.49 | 0.46 | 0.42 | 0.38 | 0.33 | 0.28 | 0.23 | 0.18 | 0.14 | 0.07 | 0.02 |
| 4° 30' | 0.48 | 0.47 | 0.45 | 0.42 | 0.39 | 0.36 | 0.32 | 0.28 | 0.24 | 0.20 | 0.16 | 0.12 | 0.06 | 0.01 |
| 5° 0' | 0.42 | 0.41 | 0.39 | 0.37 | 0.34 | 0.32 | 0.28 | 0.25 | 0.21 | 0.17 | 0.14 | 0.11 | 0.05 | 0.01 |
| 5° 30' | 0.36 | 0.35 | 0.34 | 0.32 | 0.30 | 0.27 | 0.24 | 0.21 | 0.18 | 0.15 | 0.12 | 0.09 | 0.04 | 0.01 |
| 6° 0' | 0.31 | 0.30 | 0.29 | 0.27 | 0.25 | 0.23 | 0.21 | 0.18 | 0.16 | 0.13 | 0.10 | 0.08 | 0.04 | 0.01 |
| 6° 30' | 0.27 | 0.26 | 0.25 | 0.24 | 0.22 | 0.20 | 0.18 | 0.16 | 0.14 | 0.11 | 0.09 | 0.07 | 0.03 | 0.01 |
| 7° 0' | 0.25 | 0.24 | 0.23 | 0.22 | 0.21 | 0.19 | 0.17 | 0.15 | 0.13 | 0.10 | 0.08 | 0.06 | 0.03 | 0.01 |
| 7° 30' | 0.22 | 0.21 | 0.21 | 0.19 | 0.18 | 0.17 | 0.15 | 0.13 | 0.11 | 0.09 | 0.07 | 0.06 | 0.03 | 0.01 |
| 8° 0' | 0.19 | 0.18 | 0.18 | 0.17 | 0.16 | 0.14 | 0.13 | 0.11 | 0.10 | 0.08 | 0.06 | 0.05 | 0.02 | 0.01 |
| 9° 0' | 0.16 | 0.16 | 0.15 | 0.14 | 0.13 | 0.12 | 0.11 | 0.09 | 0.08 | 0.07 | 0.05 | 0.04 | 0.02 | 0.00 |
| 10° 0' | 0.14 | 0.14 | 0.13 | 0.12 | 0.11 | 0.11 | 0.09 | 0.08 | 0.07 | 0.06 | 0.05 | 0.04 | 0.02 | 0.00 |
| 11° 0' | 0.11 | 0.11 | 0.10 | 0.10 | 0.09 | 0.08 | 0.07 | 0.06 | 0.06 | 0.05 | 0.04 | 0.03 | 0.01 | 0.00 |
| 13° 0' | 0.08 | 0.08 | 0.07 | 0.07 | 0.07 | 0.06 | 0.05 | 0.05 | 0.04 | 0.03 | 0.03 | 0.02 | 0.01 | 0.00 |
| 15° 0' | 0.06 | 0.06 | 0.06 | 0.05 | 0.05 | 0.05 | 0.04 | 0.04 | 0.03 | 0.02 | 0.02 | 0.02 | 0.01 | 0.00 |
| 20° 0' | 0.04 | 0.04 | 0.04 | 0.04 | 0.03 | 0.03 | 0.03 | 0.02 | 0.02 | 0.02 | 0.01 | 0.01 | 0.00 | 0.00 |
| 30° 0' | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.00 | 0.00 |

K

K

| | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
|-----|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| 0° | 10.2767+ | 9.67 461 | 9.07 255 | 8.72 037 | 8.47 049 | 8.27 667 | 8.11 831 | 7.98 441 | 7.86 843 | 7.76 612 |
| 1' | 7.67 461 | 7.59 182 | 7.51 625 | 7.44 672 | 7.38 235 | 7.32 243 | 7.26 637 | 7.21 371 | 7.16 406 | 7.11 710 |
| 2' | 7.07 255 | 7.03 017 | 6.98 976 | 6.95 115 | 6.91 419 | 6.87 873 | 6.84 466 | 6.81 188 | 6.78 029 | 6.74 981 |
| 3' | 6.72 037 | 6.69 188 | 6.66 431 | 6.63 758 | 6.61 165 | 6.58 647 | 6.56 200 | 6.53 820 | 6.51 504 | 6.49 248 |
| 4' | 6.47 049 | 6.44 904 | 6.42 811 | 6.40 767 | 6.38 770 | 6.36 818 | 6.34 909 | 6.33 041 | 6.31 213 | 6.29 422 |
| 5' | 6.27 667 | 6.25 947 | 6.24 260 | 6.22 606 | 6.20 982 | 6.19 388 | 6.17 823 | 6.16 286 | 6.14 775 | 6.13 290 |
| 6' | 6.11 831 | 6.10 395 | 6.08 982 | 6.07 593 | 6.06 225 | 6.04 878 | 6.03 552 | 6.02 246 | 6.00 959 | 5.99 691 |
| 7' | 5.98 441 | 5.97 209 | 5.95 994 | 5.94 796 | 5.93 614 | 5.92 449 | 5.91 298 | 5.90 163 | 5.89 042 | 5.87 935 |
| 8' | 5.86 843 | 5.85 764 | 5.84 698 | 5.83 645 | 5.82 605 | 5.81 577 | 5.80 561 | 5.79 557 | 5.78 564 | 5.77 583 |
| 9' | 5.76 612 | 5.75 653 | 5.74 703 | 5.73 764 | 5.72 835 | 5.71 916 | 5.71 007 | 5.70 106 | 5.69 216 | 5.68 334 |
| 10' | 5.67 461 | 5.66 597 | 5.65 741 | 5.64 893 | 5.64 054 | 5.63 223 | 5.62 400 | 5.61 584 | 5.60 776 | 5.59 976 |
| 11' | 5.59 182 | 5.58 396 | 5.57 617 | 5.56 845 | 5.56 080 | 5.55 321 | 5.54 569 | 5.53 824 | 5.53 084 | 5.52 351 |
| 12' | 5.51 625 | 5.50 904 | 5.50 189 | 5.49 480 | 5.48 776 | 5.48 079 | 5.47 387 | 5.46 700 | 5.46 019 | 5.45 343 |
| 13' | 5.44 672 | 5.44 007 | 5.43 346 | 5.42 691 | 5.42 040 | 5.41 394 | 5.40 753 | 5.40 117 | 5.39 485 | 5.38 858 |
| 14' | 5.38 235 | 5.37 617 | 5.37 003 | 5.36 394 | 5.35 788 | 5.35 187 | 5.34 590 | 5.33 997 | 5.33 408 | 5.32 824 |
| 15' | 5.32 243 | 5.31 665 | 5.31 092 | 5.30 523 | 5.29 957 | 5.29 395 | 5.28 836 | 5.28 281 | 5.27 729 | 5.27 181 |
| 16' | 5.26 637 | 5.26 096 | 5.25 558 | 5.25 023 | 5.24 492 | 5.23 964 | 5.23 439 | 5.22 918 | 5.22 399 | 5.21 884 |
| 17' | 5.21 371 | 5.20 862 | 5.20 355 | 5.19 852 | 5.19 351 | 5.18 853 | 5.18 358 | 5.17 866 | 5.17 377 | 5.16 890 |
| 18' | 5.16 406 | 5.15 925 | 5.15 447 | 5.14 971 | 5.14 497 | 5.14 027 | 5.13 558 | 5.13 093 | 5.12 629 | 5.12 169 |
| 19' | 5.11 710 | 5.11 254 | 5.10 801 | 5.10 349 | 5.09 901 | 5.09 454 | 5.09 010 | 5.08 568 | 5.08 128 | 5.07 690 |
| 20' | 5.07 255 | 5.06 822 | 5.06 391 | 5.05 962 | 5.05 535 | 5.05 110 | 5.04 687 | 5.04 267 | 5.03 848 | 5.03 432 |
| 21' | 5.03 017 | 5.02 604 | 5.02 194 | 5.01 785 | 5.01 378 | 5.00 973 | 5.00 570 | 5.00 169 | 4.99 770 | 4.99 372 |
| 22' | 4.98 976 | 4.98 582 | 4.98 190 | 4.97 800 | 4.97 411 | 4.97 024 | 4.96 639 | 4.96 256 | 4.95 874 | 4.95 494 |
| 23' | 4.95 115 | 4.94 739 | 4.94 363 | 4.93 990 | 4.93 618 | 4.93 247 | 4.92 879 | 4.92 511 | 4.92 146 | 4.91 781 |
| 24' | 4.91 419 | 4.91 058 | 4.90 698 | 4.90 340 | 4.89 983 | 4.89 628 | 4.89 274 | 4.88 922 | 4.88 571 | 4.88 221 |
| 25' | 4.87 873 | 4.87 526 | 4.87 181 | 4.86 837 | 4.86 494 | 4.86 153 | 4.85 813 | 4.85 474 | 4.85 137 | 4.84 801 |
| 26' | 4.84 466 | 4.84 133 | 4.83 801 | 4.83 470 | 4.83 140 | 4.82 812 | 4.82 485 | 4.82 159 | 4.81 834 | 4.81 511 |
| 27' | 4.81 188 | 4.80 867 | 4.80 547 | 4.80 228 | 4.79 911 | 4.79 594 | 4.79 279 | 4.78 965 | 4.78 652 | 4.78 340 |
| 28' | 4.78 029 | 4.77 720 | 4.77 411 | 4.77 104 | 4.76 797 | 4.76 492 | 4.76 188 | 4.75 885 | 4.75 583 | 4.75 281 |
| 29' | 4.74 981 | 4.74 682 | 4.74 384 | 4.74 088 | 4.73 792 | 4.73 497 | 4.73 203 | 4.72 910 | 4.72 618 | 4.72 327 |
| 30' | 4.72 037 | 4.71 748 | 4.71 460 | 4.71 173 | 4.70 886 | 4.70 601 | 4.70 317 | 4.70 033 | 4.69 751 | 4.69 469 |
| 31' | 4.69 189 | 4.68 909 | 4.68 630 | 4.68 352 | 4.68 075 | 4.67 799 | 4.67 524 | 4.67 249 | 4.66 976 | 4.66 703 |
| 32' | 4.66 431 | 4.66 160 | 4.65 890 | 4.65 621 | 4.65 352 | 4.65 084 | 4.64 818 | 4.64 552 | 4.64 286 | 4.64 022 |
| 33' | 4.63 758 | 4.63 496 | 4.63 233 | 4.62 972 | 4.62 712 | 4.62 452 | 4.62 193 | 4.61 935 | 4.61 678 | 4.61 421 |
| 34' | 4.61 165 | 4.60 910 | 4.60 656 | 4.60 402 | 4.60 149 | 4.59 897 | 4.59 646 | 4.59 395 | 4.59 145 | 4.58 896 |
| 35' | 4.58 648 | 4.58 400 | 4.58 153 | 4.57 906 | 4.57 661 | 4.57 415 | 4.57 171 | 4.56 928 | 4.56 685 | 4.56 442 |
| 36' | 4.56 201 | 4.55 960 | 4.55 719 | 4.55 480 | 4.55 241 | 4.55 003 | 4.54 765 | 4.54 528 | 4.54 292 | 4.54 056 |
| 37' | 4.53 821 | 4.53 586 | 4.53 353 | 4.53 119 | 4.52 887 | 4.52 655 | 4.52 424 | 4.52 193 | 4.51 963 | 4.51 733 |
| 38' | 4.51 504 | 4.51 276 | 4.51 049 | 4.50 821 | 4.50 595 | 4.50 369 | 4.50 144 | 4.49 919 | 4.49 695 | 4.49 471 |
| 39' | 4.49 248 | 4.49 026 | 4.48 804 | 4.48 583 | 4.48 362 | 4.48 142 | 4.47 922 | 4.47 703 | 4.47 485 | 4.47 267 |
| 40' | 4.47 049 | 4.46 832 | 4.46 616 | 4.46 400 | 4.46 185 | 4.45 970 | 4.45 756 | 4.45 542 | 4.45 329 | 4.45 117 |
| 41' | 4.44 905 | 4.44 693 | 4.44 482 | 4.44 271 | 4.44 061 | 4.43 852 | 4.43 643 | 4.43 434 | 4.43 226 | 4.43 019 |
| 42' | 4.42 811 | 4.42 605 | 4.42 399 | 4.42 193 | 4.41 988 | 4.41 784 | 4.41 579 | 4.41 376 | 4.41 173 | 4.40 970 |
| 43' | 4.40 768 | 4.40 566 | 4.40 365 | 4.40 164 | 4.39 963 | 4.39 764 | 4.39 564 | 4.39 365 | 4.39 167 | 4.38 968 |
| 44' | 4.38 771 | 4.38 574 | 4.38 377 | 4.38 181 | 4.37 985 | 4.37 789 | 4.37 594 | 4.37 400 | 4.37 206 | 4.37 012 |
| 45' | 4.36 819 | 4.36 626 | 4.36 434 | 4.36 242 | 4.36 050 | 4.35 859 | 4.35 668 | 4.35 478 | 4.35 288 | 4.35 099 |
| 46' | 4.34 910 | 4.34 721 | 4.34 533 | 4.34 345 | 4.34 158 | 4.33 971 | 4.33 784 | 4.33 598 | 4.33 412 | 4.33 227 |
| 47' | 4.33 042 | 4.32 857 | 4.32 673 | 4.32 489 | 4.32 306 | 4.32 123 | 4.31 940 | 4.31 758 | 4.31 576 | 4.31 394 |
| 48' | 4.31 213 | 4.31 032 | 4.30 852 | 4.30 672 | 4.30 492 | 4.30 313 | 4.30 134 | 4.29 956 | 4.29 778 | 4.29 600 |
| 49' | 4.29 422 | 4.29 245 | 4.29 068 | 4.28 892 | 4.28 716 | 4.28 540 | 4.28 365 | 4.28 190 | 4.28 016 | 4.27 841 |
| 50' | 4.27 668 | 4.27 494 | 4.27 321 | 4.27 148 | 4.26 975 | 4.26 803 | 4.26 631 | 4.26 460 | 4.26 289 | 4.26 118 |
| 51' | 4.25 948 | 4.25 777 | 4.25 608 | 4.25 438 | 4.25 269 | 4.25 100 | 4.24 932 | 4.24 763 | 4.24 596 | 4.24 428 |
| 52' | 4.24 261 | 4.24 094 | 4.23 928 | 4.23 761 | 4.23 595 | 4.23 430 | 4.23 264 | 4.23 100 | 4.22 935 | 4.22 770 |
| 53' | 4.22 606 | 4.22 443 | 4.22 279 | 4.22 116 | 4.21 953 | 4.21 791 | 4.21 629 | 4.21 467 | 4.21 305 | 4.21 144 |
| 54' | 4.20 983 | 4.20 822 | 4.20 662 | 4.20 502 | 4.20 342 | 4.20 182 | 4.20 023 | 4.19 864 | 4.19 706 | 4.19 547 |
| 55' | 4.19 389 | 4.19 231 | 4.19 074 | 4.18 917 | 4.18 760 | 4.18 603 | 4.18 447 | 4.18 291 | 4.18 135 | 4.17 979 |
| 56' | 4.17 824 | 4.17 669 | 4.17 514 | 4.17 360 | 4.17 206 | 4.17 052 | 4.16 898 | 4.16 745 | 4.16 592 | 4.16 439 |
| 57' | 4.16 287 | 4.16 135 | 4.15 983 | 4.15 831 | 4.15 679 | 4.15 528 | 4.15 377 | 4.15 227 | 4.15 076 | 4.14 926 |
| 58' | 4.14 776 | 4.14 627 | 4.14 477 | 4.14 328 | 4.14 179 | 4.14 031 | 4.13 882 | 4.13 734 | 4.13 586 | 4.13 439 |
| 59' | 4.13 291 | 4.13 144 | 4.12 998 | 4.12 851 | 4.12 705 | 4.12 558 | 4.12 413 | 4.12 267 | 4.12 122 | 4.11 977 |

Gaussians

Gaussians

| | .05 3 | .05 3 | .05 2 | .05 2 | .05 1 | .05 1 | .05 0 | .05 0 | .04 9 |
|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|-------|
| 0.87 824 99 | 0.88 253 49 | 0.88 687 99 | 0.89 124 49 | 0.89 565 99 | 0.90 011 49 | 0.90 460 99 | 0.90 913 49 | 0.91 371 99 | |
| .87 832 98 | .88 262 48 | .88 696 98 | .89 133 48 | .89 574 98 | .90 020 48 | .90 469 98 | .90 923 48 | .91 380 98 | |
| .87 841 97 | .88 271 47 | .88 704 97 | .89 142 47 | .89 583 97 | .90 028 47 | .90 478 97 | .90 932 47 | .91 390 97 | |
| .87 849 96 | .88 279 46 | .88 713 96 | .89 151 46 | .89 592 96 | .90 037 46 | .90 487 96 | .90 941 46 | .91 399 96 | |
| .87 858 95 | .88 288 45 | .88 722 95 | .89 159 45 | .89 601 95 | .90 046 45 | .90 496 95 | .90 950 45 | .91 408 95 | |
| .87 867 94 | .88 297 44 | .88 730 94 | .89 168 44 | .89 610 94 | .90 055 44 | .90 505 94 | .90 959 44 | .91 417 94 | |
| .87 875 93 | .88 305 43 | .88 739 93 | .89 177 43 | .89 619 93 | .90 064 43 | .90 514 93 | .90 968 43 | .91 426 93 | |
| .87 884 92 | .88 314 42 | .88 748 92 | .89 186 42 | .89 627 92 | .90 073 42 | .90 523 92 | .90 977 42 | .91 436 92 | |
| .87 892 91 | .88 323 41 | .88 757 91 | .89 194 41 | .89 636 91 | .90 082 41 | .90 532 91 | .90 986 41 | .91 445 91 | |
| .87 901 90 | .88 331 40 | .88 765 90 | .89 203 40 | .89 645 90 | .90 091 40 | .90 541 90 | .90 995 40 | .91 454 90 | |
| .87 909 89 | .88 340 39 | .88 774 89 | .89 212 39 | .89 654 89 | .90 100 39 | .90 550 89 | .91 005 39 | .91 463 89 | |
| .87 918 88 | .88 348 38 | .88 783 88 | .89 221 38 | .89 663 88 | .90 109 38 | .90 559 88 | .91 014 38 | .91 472 88 | |
| .87 927 87 | .88 357 37 | .88 791 87 | .89 230 37 | .89 672 87 | .90 118 37 | .90 568 87 | .91 023 37 | .91 482 87 | |
| .87 935 86 | .88 366 36 | .88 800 86 | .89 238 36 | .89 681 86 | .90 127 36 | .90 577 86 | .91 032 36 | .91 491 86 | |
| .87 944 85 | .88 374 35 | .88 809 85 | .89 247 35 | .89 690 85 | .90 136 35 | .90 586 85 | .91 041 35 | .91 500 85 | |
| .87 952 84 | .88 383 34 | .88 818 84 | .89 256 34 | .89 699 84 | .90 145 34 | .90 596 84 | .91 050 34 | .91 509 84 | |
| .87 961 83 | .88 392 33 | .88 826 83 | .89 265 33 | .89 707 83 | .90 154 33 | .90 605 83 | .91 059 33 | .91 519 83 | |
| .87 969 82 | .88 400 32 | .88 835 82 | .89 274 32 | .89 716 82 | .90 163 32 | .90 614 82 | .91 069 32 | .91 528 82 | |
| .87 978 81 | .88 409 31 | .88 844 81 | .89 283 31 | .89 725 81 | .90 172 31 | .90 623 81 | .91 078 31 | .91 537 81 | |
| .87 987 80 | .88 418 30 | .88 853 80 | .89 291 30 | .89 734 80 | .90 181 30 | .90 632 80 | .91 087 30 | .91 546 80 | |
| .87 995 79 | .88 426 29 | .88 861 79 | .89 300 29 | .89 743 79 | .90 190 29 | .90 641 79 | .91 096 29 | .91 555 79 | |
| .88 004 78 | .88 435 28 | .88 870 78 | .89 309 28 | .89 752 78 | .90 199 28 | .90 650 78 | .91 105 28 | .91 565 78 | |
| .88 012 77 | .88 444 27 | .88 879 77 | .89 318 27 | .89 761 77 | .90 208 27 | .90 659 77 | .91 114 27 | .91 574 77 | |
| .88 021 76 | .88 452 26 | .88 888 76 | .89 327 26 | .89 770 76 | .90 217 26 | .90 668 76 | .91 123 26 | .91 583 76 | |
| 0.88 030 75 | 0.88 461 25 | 0.88 896 75 | 0.89 335 25 | 0.89 779 75 | 0.90 226 25 | 0.90 677 75 | 0.91 133 25 | 0.91 592 75 | |
| .88 038 74 | .88 470 24 | .88 905 74 | .89 344 24 | .89 787 74 | .90 235 24 | .90 686 74 | .91 142 24 | .91 602 74 | |
| .88 047 73 | .88 478 23 | .88 914 73 | .89 353 23 | .89 796 73 | .90 244 23 | .90 695 73 | .91 151 23 | .91 611 73 | |
| .88 055 72 | .88 487 22 | .88 923 72 | .89 362 22 | .89 805 72 | .90 253 22 | .90 704 72 | .91 160 22 | .91 620 72 | |
| .88 064 71 | .88 496 21 | .88 931 71 | .89 371 21 | .89 814 71 | .90 262 21 | .90 713 71 | .91 169 21 | .91 629 71 | |
| .88 073 70 | .88 504 20 | .88 940 70 | .89 380 20 | .89 823 70 | .90 271 20 | .90 722 70 | .91 178 20 | .91 639 70 | |
| .88 081 69 | .88 513 19 | .88 949 69 | .89 388 19 | .89 832 69 | .90 280 19 | .90 732 69 | .91 188 19 | .91 648 69 | |
| .88 090 68 | .88 522 18 | .88 958 68 | .89 397 18 | .89 841 68 | .90 289 18 | .90 741 68 | .91 197 18 | .91 657 68 | |
| .88 098 67 | .88 530 17 | .88 966 67 | .89 406 17 | .89 850 67 | .90 298 17 | .90 750 67 | .91 206 17 | .91 666 67 | |
| .88 107 66 | .88 539 16 | .88 975 66 | .89 415 16 | .89 859 66 | .90 307 16 | .90 759 66 | .91 215 16 | .91 676 66 | |
| .88 116 65 | .88 548 15 | .88 984 65 | .89 424 15 | .89 868 65 | .90 316 15 | .90 768 65 | .91 224 15 | .91 685 65 | |
| .88 124 64 | .88 556 14 | .88 993 64 | .89 433 14 | .89 877 64 | .90 325 14 | .90 777 64 | .91 233 14 | .91 694 64 | |
| .88 133 63 | .88 565 13 | .89 001 63 | .89 441 13 | .89 886 63 | .90 334 13 | .90 786 63 | .91 243 13 | .91 703 63 | |
| .88 141 62 | .88 574 12 | .89 010 62 | .89 450 12 | .89 894 62 | .90 343 12 | .90 795 62 | .91 252 12 | .91 713 62 | |
| .88 150 61 | .88 582 11 | .89 019 61 | .89 459 11 | .89 903 61 | .90 352 11 | .90 804 61 | .91 261 11 | .91 722 61 | |
| .88 159 60 | .88 591 10 | .89 028 60 | .89 468 10 | .89 912 60 | .90 361 10 | .90 813 60 | .91 270 10 | .91 731 60 | |
| .88 167 59 | .88 600 09 | .89 036 59 | .89 477 09 | .89 921 59 | .90 370 09 | .90 822 59 | .91 279 09 | .91 740 59 | |
| .88 176 58 | .88 609 08 | .89 045 58 | .89 486 08 | .89 930 58 | .90 379 08 | .90 831 58 | .91 288 08 | .91 750 58 | |
| .88 184 57 | .88 617 07 | .89 054 57 | .89 495 07 | .89 939 57 | .90 388 07 | .90 841 57 | .91 298 07 | .91 759 57 | |
| .88 193 56 | .88 626 06 | .89 063 56 | .89 503 06 | .89 948 56 | .90 397 06 | .90 850 56 | .91 307 06 | .91 768 56 | |
| .88 202 55 | .88 635 05 | .89 071 55 | .89 512 05 | .89 957 55 | .90 406 05 | .90 859 55 | .91 316 05 | .91 778 55 | |
| .88 210 54 | .88 643 04 | .89 080 54 | .89 521 04 | .89 966 54 | .90 415 04 | .90 868 54 | .91 325 04 | .91 787 54 | |
| .88 219 53 | .88 652 03 | .89 089 53 | .89 530 03 | .89 975 53 | .90 424 03 | .90 877 53 | .91 334 03 | .91 796 53 | |
| .88 228 52 | .88 661 02 | .89 098 52 | .89 539 02 | .89 984 52 | .90 433 02 | .90 886 52 | .91 344 02 | .91 805 52 | |
| .88 236 51 | .88 669 01 | .89 107 51 | .89 548 01 | .89 993 51 | .90 442 01 | .90 895 51 | .91 353 01 | .91 815 51 | |
| 0.88 245 50 | 0.88 678 00 | 0.89 115 50 | 0.89 556 00 | 0.90 002 50 | 0.90 451 00 | 0.90 904 50 | 0.91 362 00 | 0.91 824 50 | |

Find your entering number in the column of heavy print. If there isn't a perfect match, go to the next larger number. The last part of the gaussian is beside it; the first part is above the column.

Table 7

| 0° | .0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 |
|-----|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0' | | 3.3802 | 3.0792 | 2.9031 | 2.7782 | 2.6812 | 2.6021 | 2.5351 | 2.4771 | 2.4260 |
| 1' | 2.3802 | 2.3388 | 2.3010 | 2.2663 | 2.2341 | 2.2041 | 2.1761 | 2.1498 | 2.1249 | 2.1015 |
| 2' | 2.0792 | 2.0580 | 2.0378 | 2.0185 | 2.0000 | 1.9823 | 1.9652 | 1.9488 | 1.9331 | 1.9178 |
| 3' | 1.9031 | 1.8888 | 1.8751 | 1.8617 | 1.8487 | 1.8361 | 1.8239 | 1.8120 | 1.8004 | 1.7891 |
| 4' | 1.7782 | 1.7674 | 1.7570 | 1.7467 | 1.7368 | 1.7270 | 1.7175 | 1.7081 | 1.6990 | 1.6900 |
| 5' | 1.6812 | 1.6726 | 1.6642 | 1.6559 | 1.6478 | 1.6398 | 1.6320 | 1.6243 | 1.6168 | 1.6094 |
| 6' | 1.6021 | 1.5949 | 1.5878 | 1.5809 | 1.5740 | 1.5673 | 1.5607 | 1.5541 | 1.5477 | 1.5414 |
| 7' | 1.5351 | 1.5290 | 1.5229 | 1.5169 | 1.5110 | 1.5051 | 1.4994 | 1.4937 | 1.4881 | 1.4826 |
| 8' | 1.4771 | 1.4717 | 1.4664 | 1.4611 | 1.4559 | 1.4508 | 1.4457 | 1.4407 | 1.4357 | 1.4308 |
| 9' | 1.4260 | 1.4212 | 1.4164 | 1.4117 | 1.4071 | 1.4025 | 1.3979 | 1.3934 | 1.3890 | 1.3846 |
| 10' | 1.3802 | 1.3759 | 1.3716 | 1.3674 | 1.3632 | 1.3590 | 1.3549 | 1.3508 | 1.3468 | 1.3428 |
| 11' | 1.3388 | 1.3349 | 1.3310 | 1.3271 | 1.3233 | 1.3195 | 1.3158 | 1.3120 | 1.3083 | 1.3047 |
| 12' | 1.3010 | 1.2974 | 1.2939 | 1.2903 | 1.2868 | 1.2833 | 1.2798 | 1.2764 | 1.2730 | 1.2696 |
| 13' | 1.2663 | 1.2629 | 1.2596 | 1.2564 | 1.2531 | 1.2499 | 1.2467 | 1.2435 | 1.2403 | 1.2372 |
| 14' | 1.2341 | 1.2310 | 1.2279 | 1.2249 | 1.2218 | 1.2188 | 1.2159 | 1.2129 | 1.2099 | 1.2070 |
| 15' | 1.2041 | 1.2012 | 1.1984 | 1.1955 | 1.1927 | 1.1899 | 1.1871 | 1.1843 | 1.1816 | 1.1788 |
| 16' | 1.1761 | 1.1734 | 1.1707 | 1.1680 | 1.1654 | 1.1627 | 1.1601 | 1.1575 | 1.1549 | 1.1523 |
| 17' | 1.1498 | 1.1472 | 1.1447 | 1.1422 | 1.1397 | 1.1372 | 1.1347 | 1.1322 | 1.1298 | 1.1274 |
| 18' | 1.1249 | 1.1225 | 1.1201 | 1.1178 | 1.1154 | 1.1130 | 1.1107 | 1.1084 | 1.1061 | 1.1037 |
| 19' | 1.1015 | 1.0992 | 1.0969 | 1.0947 | 1.0924 | 1.0902 | 1.0880 | 1.0857 | 1.0835 | 1.0814 |
| 20' | 1.0792 | 1.0770 | 1.0749 | 1.0727 | 1.0706 | 1.0685 | 1.0663 | 1.0642 | 1.0621 | 1.0601 |
| 21' | 1.0580 | 1.0559 | 1.0539 | 1.0518 | 1.0498 | 1.0478 | 1.0458 | 1.0438 | 1.0418 | 1.0398 |
| 22' | 1.0378 | 1.0358 | 1.0339 | 1.0319 | 1.0300 | 1.0280 | 1.0261 | 1.0242 | 1.0223 | 1.0204 |
| 23' | 1.0185 | 1.0166 | 1.0147 | 1.0129 | 1.0110 | 1.0091 | 1.0073 | 1.0055 | 1.0036 | 1.0018 |
| 24' | 1.0000 | 0.9982 | 0.9964 | 0.9946 | 0.9928 | 0.9910 | 0.9893 | 0.9875 | 0.9858 | 0.9840 |
| 25' | 0.9823 | 0.9805 | 0.9788 | 0.9771 | 0.9754 | 0.9737 | 0.9720 | 0.9703 | 0.9686 | 0.9669 |
| 26' | 0.9652 | 0.9636 | 0.9619 | 0.9603 | 0.9586 | 0.9570 | 0.9553 | 0.9537 | 0.9521 | 0.9505 |
| 27' | 0.9488 | 0.9472 | 0.9456 | 0.9440 | 0.9425 | 0.9409 | 0.9393 | 0.9377 | 0.9362 | 0.9346 |
| 28' | 0.9331 | 0.9315 | 0.9300 | 0.9284 | 0.9269 | 0.9254 | 0.9238 | 0.9223 | 0.9208 | 0.9193 |
| 29' | 0.9178 | 0.9163 | 0.9148 | 0.9133 | 0.9119 | 0.9104 | 0.9089 | 0.9075 | 0.9060 | 0.9045 |
| 30' | 0.9031 | 0.9016 | 0.9002 | 0.8988 | 0.8973 | 0.8959 | 0.8945 | 0.8931 | 0.8917 | 0.8903 |
| 31' | 0.8888 | 0.8875 | 0.8861 | 0.8847 | 0.8833 | 0.8819 | 0.8805 | 0.8792 | 0.8778 | 0.8764 |
| 32' | 0.8751 | 0.8737 | 0.8724 | 0.8710 | 0.8697 | 0.8683 | 0.8670 | 0.8657 | 0.8643 | 0.8630 |
| 33' | 0.8617 | 0.8604 | 0.8591 | 0.8578 | 0.8565 | 0.8552 | 0.8539 | 0.8526 | 0.8513 | 0.8500 |
| 34' | 0.8487 | 0.8475 | 0.8462 | 0.8449 | 0.8437 | 0.8424 | 0.8411 | 0.8399 | 0.8386 | 0.8374 |
| 35' | 0.8361 | 0.8349 | 0.8337 | 0.8324 | 0.8312 | 0.8300 | 0.8288 | 0.8275 | 0.8263 | 0.8251 |
| 36' | 0.8239 | 0.8227 | 0.8215 | 0.8203 | 0.8191 | 0.8179 | 0.8167 | 0.8155 | 0.8144 | 0.8132 |
| 37' | 0.8120 | 0.8108 | 0.8097 | 0.8085 | 0.8073 | 0.8062 | 0.8050 | 0.8039 | 0.8027 | 0.8016 |
| 38' | 0.8004 | 0.7993 | 0.7981 | 0.7970 | 0.7959 | 0.7948 | 0.7936 | 0.7925 | 0.7914 | 0.7903 |
| 39' | 0.7891 | 0.7880 | 0.7869 | 0.7858 | 0.7847 | 0.7836 | 0.7825 | 0.7814 | 0.7803 | 0.7792 |
| 40' | 0.7782 | 0.7771 | 0.7760 | 0.7749 | 0.7738 | 0.7728 | 0.7717 | 0.7706 | 0.7696 | 0.7685 |
| 41' | 0.7674 | 0.7664 | 0.7653 | 0.7643 | 0.7632 | 0.7622 | 0.7611 | 0.7601 | 0.7590 | 0.7580 |
| 42' | 0.7570 | 0.7559 | 0.7549 | 0.7539 | 0.7528 | 0.7518 | 0.7508 | 0.7498 | 0.7488 | 0.7478 |
| 43' | 0.7467 | 0.7457 | 0.7447 | 0.7437 | 0.7427 | 0.7417 | 0.7407 | 0.7397 | 0.7387 | 0.7377 |
| 44' | 0.7368 | 0.7358 | 0.7348 | 0.7338 | 0.7328 | 0.7319 | 0.7309 | 0.7299 | 0.7289 | 0.7280 |
| 45' | 0.7270 | 0.7260 | 0.7251 | 0.7241 | 0.7232 | 0.7222 | 0.7212 | 0.7203 | 0.7193 | 0.7184 |
| 46' | 0.7175 | 0.7165 | 0.7156 | 0.7146 | 0.7137 | 0.7128 | 0.7118 | 0.7109 | 0.7100 | 0.7090 |
| 47' | 0.7081 | 0.7072 | 0.7063 | 0.7054 | 0.7044 | 0.7035 | 0.7026 | 0.7017 | 0.7008 | 0.6999 |
| 48' | 0.6990 | 0.6981 | 0.6972 | 0.6963 | 0.6954 | 0.6945 | 0.6936 | 0.6927 | 0.6918 | 0.6909 |
| 49' | 0.6900 | 0.6891 | 0.6882 | 0.6874 | 0.6865 | 0.6856 | 0.6847 | 0.6839 | 0.6830 | 0.6821 |
| 50' | 0.6812 | 0.6804 | 0.6795 | 0.6786 | 0.6778 | 0.6769 | 0.6761 | 0.6752 | 0.6743 | 0.6735 |
| 51' | 0.6726 | 0.6718 | 0.6709 | 0.6701 | 0.6692 | 0.6684 | 0.6676 | 0.6667 | 0.6659 | 0.6650 |
| 52' | 0.6642 | 0.6634 | 0.6625 | 0.6617 | 0.6609 | 0.6601 | 0.6592 | 0.6584 | 0.6576 | 0.6568 |
| 53' | 0.6559 | 0.6551 | 0.6543 | 0.6535 | 0.6527 | 0.6519 | 0.6510 | 0.6502 | 0.6494 | 0.6486 |
| 54' | 0.6478 | 0.6470 | 0.6462 | 0.6454 | 0.6446 | 0.6438 | 0.6430 | 0.6422 | 0.6414 | 0.6406 |
| 55' | 0.6398 | 0.6391 | 0.6383 | 0.6375 | 0.6367 | 0.6359 | 0.6351 | 0.6344 | 0.6336 | 0.6328 |
| 56' | 0.6320 | 0.6312 | 0.6305 | 0.6297 | 0.6289 | 0.6282 | 0.6274 | 0.6266 | 0.6259 | 0.6251 |
| 57' | 0.6243 | 0.6236 | 0.6228 | 0.6221 | 0.6213 | 0.6205 | 0.6198 | 0.6190 | 0.6183 | 0.6175 |
| 58' | 0.6168 | 0.6160 | 0.6153 | 0.6145 | 0.6138 | 0.6131 | 0.6123 | 0.6116 | 0.6108 | 0.6101 |
| 59' | 0.6094 | 0.6086 | 0.6079 | 0.6072 | 0.6064 | 0.6057 | 0.6050 | 0.6042 | 0.6035 | 0.6028 |

Table 7

0°

Appendix

Using Predicted Lunar Distances

The tables and procedures presented in this book are self contained, and do not require other data beyond what is included in present day almanacs of the bodies being used (GHA, Dec, HP). The lunar sight reduction process, however, can be notably quicker when pre-computed lunar distance data are available.

In the early days of celestial navigation when lunars were part of the routine, the Nautical Almanac and other publications included computed lunar distances that could be used to both predict the best sights to take and to evaluate the actual sights once taken. The most common format for these predictions gave the distances every 3 hours for the selected bodies that would yield the best lunar sights.

These data have not been available from official government sources since about 1905, but several individuals have provided these predictions each year for several years now, and thus the data are once again readily available to mariners. Notable examples of this work include that of Steven Wepster of the University of Utrecht and Frank Reed, coordinator of the NavList discussion group (www.fer3.com/arc), which specializes in lunar theory and practice among many other topics. Examples from each source are shown below.

JULY 2010

| | ° / P.L. | ° / P.L. | ° / P.L. | ° / P.L. | ° / P.L. |
|-------------|--------------------|---------------|-----------------|---------------|--------------|
| 4 UT | +Kaus Aust. | +Nunki | +Jupiter | -Hamal | -Sun |
| 0 | 90 55.2 3071 | 82 58.1 3007 | 6 57.6 6619 | 32 42.0 3063 | 96 45.8 3356 |
| 3 | 92 23.9 3063 | 84 28.1 2999 | 7 36.8 5374 | 31 13.1 3061 | 95 22.7 3347 |
| 6 | 93 52.8 3054 | 85 58.4 2990 | 8 29.0 4644 | 29 44.2 3059 | 93 59.4 3337 |
| 9 | 95 21.9 3045 | 87 28.8 2980 | 9 30.7 4186 | 28 15.2 3057 | 92 35.9 3327 |
| 12 | 96 51.2 3036 | 88 59.4 2971 | 10 39.4 3883 | 26 46.2 3058 | 91 12.3 3317 |
| 15 | 98 20.7 3026 | 90 30.2 2960 | 11 53.0 3671 | 25 17.2 3058 | 89 48.4 3306 |
| 18 | 99 50.3 3016 | 92 1.2 2950 | 13 10.3 3519 | 23 48.2 3061 | 88 24.3 3294 |
| 21 | 101 20.2 3006 | 93 32.5 2939 | 14 30.3 3405 | 22 19.2 3067 | 87 0.0 3282 |

Sample data from Steve Wepster, available at www.staff.science.uu.nl/~wepst101/tables.html (archived at www.starpath.com/navpubs). He offers distances to the best five bodies, at 3-hour intervals each day. The data are presented in print ready pdf documents.

| Lunars Almanac for July 4, 2010, Date and Times are GMT. | | | | | | | | |
|--|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|
| | 0:00 | 3:00 | 6:00 | 9:00 | 12:00 | 15:00 | 18:00 | 21:00 |
| Moon's HP | 54.65 | 54.71 | 54.77 | 54.83 | 54.88 | 54.95 | 55.02 | 55.08 |
| Sun SD: | 15.74 | | | | | | | |
| The Sun | 96° 45.8' | 95° 22.7' | 93° 59.4' | 92° 36.0' | 91° 12.3' | 89° 48.4' | 88° 24.4' | 87° 00.0' |
| Jupiter | --- | --- | --- | --- | 10° 39.4' | 11° 53.0' | 13° 10.3' | 14° 30.3' |
| Hamal | 32° 42.1' | 31° 13.2' | 29° 44.2' | 28° 15.2' | 26° 46.2' | 25° 17.2' | 23° 48.2' | 22° 19.3' |
| Kaus Aust. | 90° 55.1' | 92° 23.9' | 93° 52.8' | 95° 21.9' | 96° 51.1' | 98° 20.6' | 99° 50.3' | 101° 20.2' |
| Nunki | 82° 58.0' | 84° 28.1' | 85° 58.3' | 87° 28.8' | 88° 59.4' | 90° 30.2' | 92° 01.2' | 93° 32.5' |

Sample data from Frank Reed, available at www.historicalatlas.com/lunars/lunars_pre_v5.html (archived at www.starpath.com/navpubs). He offers data for all reasonable bodies at 1-, 2-, or 3-hour intervals each day. The above is an excerpt to compare with the Wepster format. The data are presented as web-page tables, covering the bodies chosen by the user.

Prior to an ocean voyage or terrestrial expedition, the navigator can quickly print out these tables for the dates underway and use them as called for to expedite the lunar process.

The traditional way to interpolate predicted distances data for the actual distance observed makes use of Proportional Logarithms. For convenience to the navigator, a set of these tables, customized to this application, along with instructions on using them is included in this Appendix.

Proportional Logarithms

Degree:minute, or Hour:minute

| | 0:00 | 0:01 | 0:02 | 0:03 | 0:04 | 0:05 | 0:06 | 0:07 | 0:08 | 0:09 | 0:10 | 0:11 | 0:12 | 0:13 | 0:14 | 0:15 | 0:16 | 0:17 |
|----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| S | 2.2553 | 1.9542 | 1.7782 | 1.6532 | 1.5563 | 1.4771 | 1.4102 | 1.3522 | 1.3010 | 1.2553 | 1.2139 | 1.1761 | 1.1413 | 1.1091 | 1.0792 | 1.0512 | 1.0248 | |
| E | 3.7324 | 2.2410 | 1.9471 | 1.7734 | 1.6496 | 1.5534 | 1.4747 | 1.4081 | 1.3504 | 1.2994 | 1.2538 | 1.2126 | 1.1749 | 1.1402 | 1.1081 | 1.0782 | 1.0502 | 1.0240 |
| C | 3.4314 | 2.2272 | 1.9400 | 1.7686 | 1.6460 | 1.5506 | 1.4723 | 1.4061 | 1.3486 | 1.2978 | 1.2524 | 1.2113 | 1.1737 | 1.1391 | 1.1071 | 1.0773 | 1.0493 | 1.0231 |
| A | 3.2553 | 2.2139 | 1.9331 | 1.7639 | 1.6425 | 1.5477 | 1.4699 | 1.4040 | 1.3468 | 1.2962 | 1.2510 | 1.2099 | 1.1725 | 1.1380 | 1.1061 | 1.0763 | 1.0484 | 1.0223 |
| R | 3.1303 | 2.2009 | 1.9262 | 1.7593 | 1.6390 | 1.5449 | 1.4676 | 1.4020 | 1.3450 | 1.2946 | 1.2495 | 1.2086 | 1.1713 | 1.1369 | 1.1050 | 1.0753 | 1.0475 | 1.0214 |
| O | 3.0334 | 2.1883 | 1.9195 | 1.7547 | 1.6355 | 1.5421 | 1.4652 | 1.4000 | 1.3432 | 1.2931 | 1.2481 | 1.2073 | 1.1701 | 1.1358 | 1.1040 | 1.0744 | 1.0467 | 1.0206 |
| F | 2.9542 | 2.1761 | 1.9128 | 1.7501 | 1.6320 | 1.5393 | 1.4629 | 1.3979 | 1.3415 | 1.2915 | 1.2467 | 1.2061 | 1.1689 | 1.1347 | 1.1030 | 1.0734 | 1.0458 | 1.0197 |
| I | 2.8873 | 2.1642 | 1.9063 | 1.7456 | 1.6286 | 1.5365 | 1.4606 | 1.3959 | 1.3397 | 1.2899 | 1.2453 | 1.2048 | 1.1677 | 1.1336 | 1.1020 | 1.0725 | 1.0449 | 1.0189 |
| M | 2.8293 | 2.1526 | 1.8999 | 1.7412 | 1.6252 | 1.5337 | 1.4582 | 1.3939 | 1.3379 | 1.2883 | 1.2438 | 1.2035 | 1.1665 | 1.1325 | 1.1009 | 1.0715 | 1.0440 | 1.0181 |
| E | 2.7782 | 2.1413 | 1.8935 | 1.7368 | 1.6218 | 1.5310 | 1.4559 | 1.3919 | 1.3362 | 1.2868 | 1.2424 | 1.2022 | 1.1654 | 1.1314 | 1.0999 | 1.0706 | 1.0431 | 1.0172 |
| T | 2.7324 | 2.1303 | 1.8873 | 1.7324 | 1.6185 | 1.5283 | 1.4536 | 1.3900 | 1.3345 | 1.2852 | 1.2410 | 1.2009 | 1.1642 | 1.1303 | 1.0989 | 1.0696 | 1.0422 | 1.0164 |
| R | 2.6910 | 2.1196 | 1.8811 | 1.7281 | 1.6151 | 1.5256 | 1.4514 | 1.3880 | 1.3327 | 1.2837 | 1.2396 | 1.1996 | 1.1630 | 1.1292 | 1.0979 | 1.0687 | 1.0413 | 1.0156 |
| O | 2.6532 | 2.1091 | 1.8751 | 1.7238 | 1.6118 | 1.5229 | 1.4491 | 1.3860 | 1.3310 | 1.2821 | 1.2382 | 1.1984 | 1.1619 | 1.1282 | 1.0969 | 1.0678 | 1.0404 | 1.0147 |
| F | 2.6185 | 2.0989 | 1.8691 | 1.7196 | 1.6085 | 1.5202 | 1.4468 | 1.3841 | 1.3293 | 1.2806 | 1.2368 | 1.1971 | 1.1607 | 1.1271 | 1.0959 | 1.0668 | 1.0395 | 1.0139 |
| I | 2.5863 | 2.0889 | 1.8632 | 1.7154 | 1.6053 | 1.5175 | 1.4446 | 1.3821 | 1.3276 | 1.2791 | 1.2355 | 1.1958 | 1.1595 | 1.1260 | 1.0949 | 1.0659 | 1.0387 | 1.0131 |
| M | 2.5563 | 2.0792 | 1.8573 | 1.7112 | 1.6021 | 1.5149 | 1.4424 | 1.3802 | 1.3259 | 1.2775 | 1.2341 | 1.1946 | 1.1584 | 1.1249 | 1.0939 | 1.0649 | 1.0378 | 1.0122 |
| E | 2.5283 | 2.0696 | 1.8516 | 1.7071 | 1.5989 | 1.5123 | 1.4401 | 1.3783 | 1.3242 | 1.2760 | 1.2327 | 1.1933 | 1.1572 | 1.1239 | 1.0929 | 1.0640 | 1.0369 | 1.0114 |
| R | 2.5019 | 2.0603 | 1.8459 | 1.7030 | 1.5957 | 1.5097 | 1.4379 | 1.3764 | 1.3225 | 1.2745 | 1.2313 | 1.1921 | 1.1561 | 1.1228 | 1.0919 | 1.0631 | 1.0360 | 1.0106 |
| O | 2.4771 | 2.0512 | 1.8403 | 1.6990 | 1.5925 | 1.5071 | 1.4357 | 1.3745 | 1.3208 | 1.2730 | 1.2300 | 1.1908 | 1.1549 | 1.1217 | 1.0909 | 1.0621 | 1.0352 | 1.0098 |
| F | 2.4536 | 2.0422 | 1.8348 | 1.6950 | 1.5894 | 1.5045 | 1.4335 | 1.3726 | 1.3191 | 1.2715 | 1.2286 | 1.1896 | 1.1538 | 1.1207 | 1.0899 | 1.0612 | 1.0343 | 1.0089 |
| I | 2.4314 | 2.0334 | 1.8293 | 1.6910 | 1.5863 | 1.5019 | 1.4314 | 1.3707 | 1.3174 | 1.2700 | 1.2272 | 1.1883 | 1.1526 | 1.1196 | 1.0889 | 1.0603 | 1.0334 | 1.0081 |
| M | 2.4102 | 2.0248 | 1.8239 | 1.6871 | 1.5832 | 1.4994 | 1.4292 | 1.3688 | 1.3158 | 1.2685 | 1.2259 | 1.1871 | 1.1515 | 1.1186 | 1.0880 | 1.0594 | 1.0326 | 1.0073 |
| E | 2.3900 | 2.0164 | 1.8186 | 1.6832 | 1.5801 | 1.4969 | 1.4270 | 1.3669 | 1.3141 | 1.2670 | 1.2245 | 1.1859 | 1.1503 | 1.1175 | 1.0870 | 1.0585 | 1.0317 | 1.0065 |
| R | 2.3707 | 2.0081 | 1.8133 | 1.6793 | 1.5771 | 1.4943 | 1.4249 | 1.3650 | 1.3124 | 1.2655 | 1.2232 | 1.1846 | 1.1492 | 1.1164 | 1.0860 | 1.0575 | 1.0308 | 1.0057 |
| O | 2.3522 | 2.0000 | 1.8081 | 1.6755 | 1.5740 | 1.4918 | 1.4228 | 1.3632 | 1.3108 | 1.2640 | 1.2218 | 1.1834 | 1.1481 | 1.1154 | 1.0850 | 1.0566 | 1.0300 | 1.0049 |
| F | 2.3345 | 1.9920 | 1.8030 | 1.6717 | 1.5710 | 1.4894 | 1.4206 | 1.3613 | 1.3091 | 1.2626 | 1.2205 | 1.1822 | 1.1469 | 1.1143 | 1.0840 | 1.0557 | 1.0291 | 1.0040 |
| I | 2.3174 | 1.9842 | 1.7979 | 1.6679 | 1.5680 | 1.4869 | 1.4185 | 1.3595 | 1.3075 | 1.2611 | 1.2192 | 1.1809 | 1.1458 | 1.1133 | 1.0831 | 1.0548 | 1.0282 | 1.0032 |
| M | 2.3010 | 1.9765 | 1.7929 | 1.6642 | 1.5651 | 1.4844 | 1.4164 | 1.3576 | 1.3059 | 1.2596 | 1.2178 | 1.1797 | 1.1447 | 1.1123 | 1.0821 | 1.0539 | 1.0274 | 1.0024 |
| E | 2.2852 | 1.9690 | 1.7879 | 1.6605 | 1.5621 | 1.4820 | 1.4143 | 1.3558 | 1.3043 | 1.2582 | 1.2165 | 1.1785 | 1.1436 | 1.1112 | 1.0811 | 1.0530 | 1.0265 | 1.0016 |
| R | 2.2700 | 1.9615 | 1.7830 | 1.6568 | 1.5592 | 1.4795 | 1.4122 | 1.3540 | 1.3026 | 1.2567 | 1.2152 | 1.1773 | 1.1424 | 1.1102 | 1.0801 | 1.0521 | 1.0257 | 1.0008 |

A R C

Lunar distance between Jupiter and the Moon



Celestial navigation is a way to find your latitude and longitude on earth using a sextant to measure the angular heights of celestial bodies above the horizon. It has been used by mariners at sea and explorers on land for three hundred years, and it is still used today as a dependable backup to modern electronic navigation.

Routine celestial navigation relies upon accurate time (Universal Time) to find the longitude of a position (latitude does not require time). Advanced celestial navigators can find longitude *without knowing the time* using a technique called Lunar Distance. In this technique, the sextant is used to measure the angular (diagonal) distance between the moon and another celestial body. Since this distance slowly changes as the moon moves eastward through the stars, it can be used to find Universal Time, which is needed to complete the longitude determination.

The process of finding longitude from lunar distance, however, requires special tables that have not been published in the *Nautical Almanac* or other sources since the early 1900s. Although software solutions are now available, most advanced celestial navigators are very grateful to navigation historian Bruce Stark for creating these printed tables dedicated to this task. They have been used and tested by mariners for more than 15 years and are praised by experts for their ingenuity and ease of use in solving this complex navigation exercise—which all agree is the hallmark of an expert celestial navigator.

With *The Stark Tables* in your nav station, you no longer have to fear losing power to your electronic navigation aids, nor are you dependent on accurate time from any official broadcast.

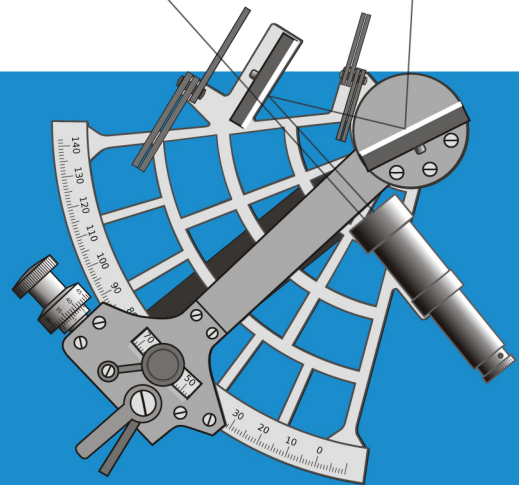
Besides their practical use in back up navigation, historians have used these tables for years to interpret the logbooks of Lewis and Clark, David Thompson, James Cook, Matthew Flinders, George Vancouver, Nathaniel Bowditch, and other notable explorers and sea captains.

“Captain Cook would have relished using these tables, had they been available to him then.”

— George Huxtable, FRIN

“It is remarkable in this day when the very survival of celestial navigation seems in question, that an individual should suddenly appear on the scene and present to the world such a brilliant piece of work. Stark has rendered a great service to the celestial navigation community.”

— Robert Eno, *The Navigator's Newsletter*



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